

Tableau 1 – Limites pour les appareils de classe A

Rang harmonique n	Courant harmonique maximal autorisé A
Harmoniques impairs	
3	2,30
5	1,14
7	0,77
9	0,40
11	0,33
13	0,21
$15 \leq n \leq 39$	$0,15 \frac{15}{n}$
Harmoniques pairs	
2	1,08
4	0,43
6	0,30
$8 \leq n \leq 40$	$0,23 \frac{8}{n}$

Tableau 2 – Limites pour les appareils de classe C

Rang harmonique n	Courant harmonique maximal exprimé en pourcentage du courant fondamental d'entrée des luminaires %
2	2
3	$30 \cdot \lambda^*$
5	10
7	7
9	5
$11 \leq n \leq 39$ (harmoniques impairs seulement)	3

* λ est le facteur de puissance du circuit

Tableau 3 – Limites pour les appareils de classe D

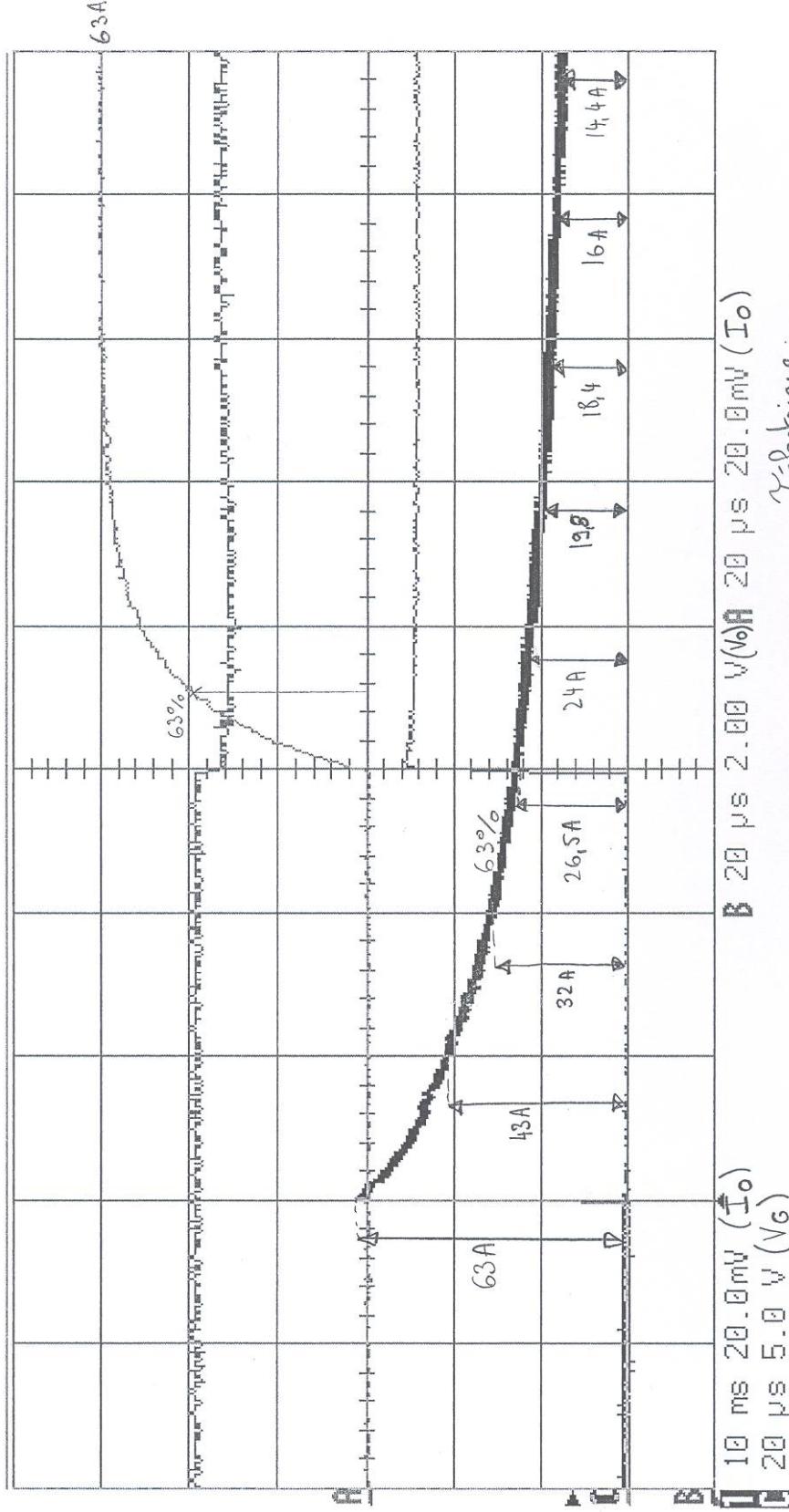
Rang harmonique n	Courant harmonique maximal autorisé par watt mA/W	Courant harmonique maximal autorisé A
3	3,4	2,30
5	1,9	1,14
7	1,0	0,77
9	0,5	0,40
11	0,35	0,33
$13 \leq n \leq 39$ (harmoniques impairs seulement)	$\frac{3,85}{n}$	Voir tableau 1

- Alimentation 6tN 30-50 Allumage à l'oid

- Alimentation Gt N 30 -
- Interruptions no-bounds

Allomage à l'void

Annexe



```

mean(1)    24.58 mV
maximum(1) 63.1 mV
mean(2)    28.492 V
maximum(2) 65.218 V
mean(3)    35.571 V
maximum(3) 75.678 V
mean(4)    42.726 V
maximum(4) 80.836 V

```

$$\frac{\Upsilon_{\text{thermique}}}{\Upsilon_{\text{th}}} = 2 \cdot 10 \text{ ms}$$

$$\frac{t_{\text{thermique}}}{T_{\text{th}}} = 2 \cdot 10 \text{ ms} = 20 \text{ ms}$$

Télétrique :

$$20,5 \text{ mm} = 20 \mu\text{s}$$

$$10,1 \text{ mm} = 9,853 \text{ } \mu\text{s} = 1\text{-}\mu\text{s}$$

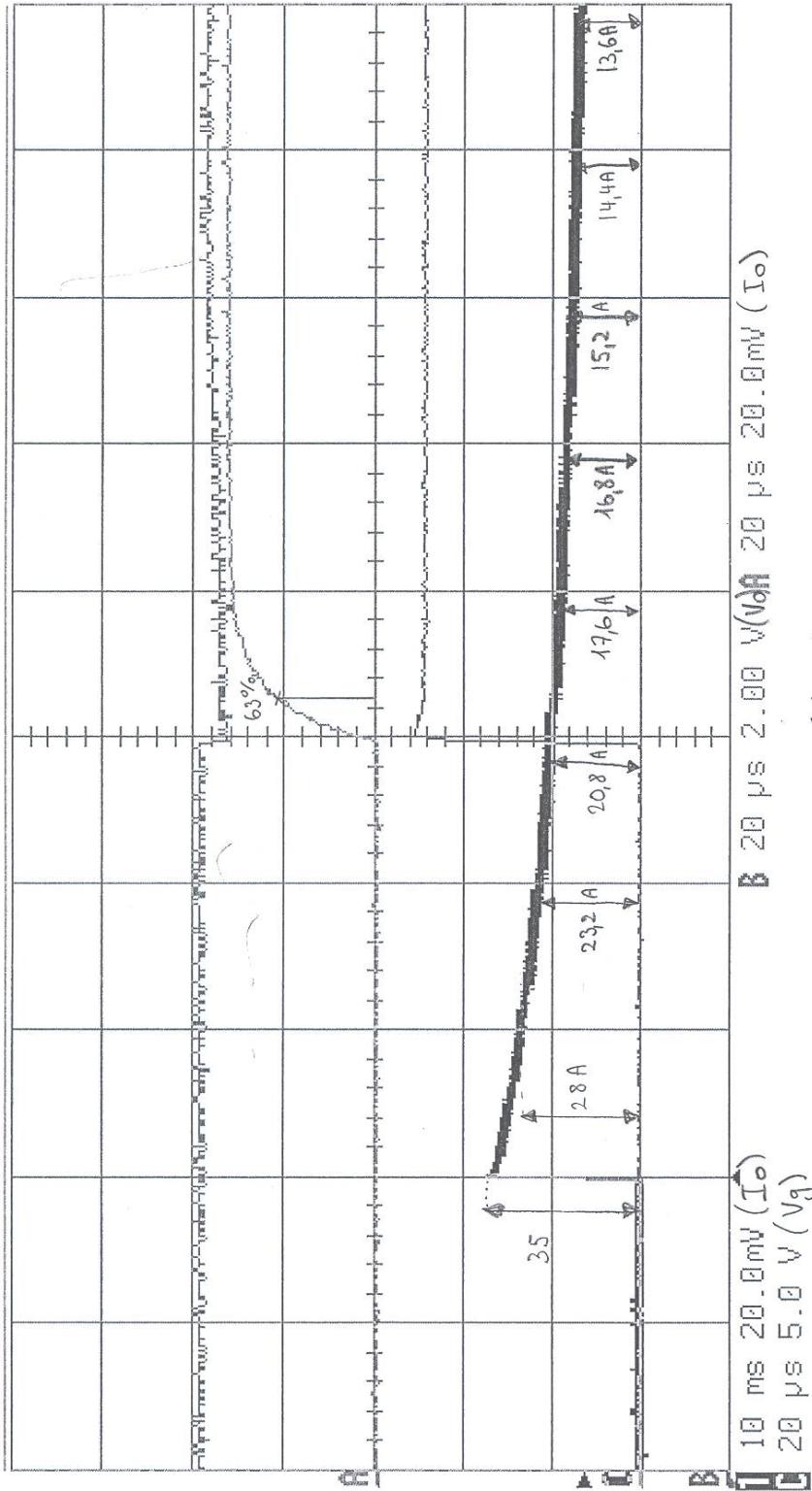
$$\textcircled{2} \quad 15,07 \mu\Omega = 1,4 \gamma$$

$$\tau_{\text{ep}_2} = 10,764 \text{ } \mu\text{s}$$

$$m = 10^4 \text{ g} \cdot \text{mol}^{-1}$$

Allumage avec préchauffage :

Annexe 3



Électrique :

mesure 1 :
 tension (1) : 10.19 mV (A)
 tension (2) : 25.8 mV
 tension (3) : 48.55 mV
 tension (4) : 52.2 mV
 tension (5) : 57.36 mV = 1.4 V

mesure 2 :
 tension (1) : 10.20 mV (A)

mesure 3 :
 tension (1) : 10.19 mV (A)
 tension (2) : 25.8 mV
 tension (3) : 48.55 mV
 tension (4) : 52.2 mV
 tension (5) : 57.36 mV = 1.4 V

$$\left. \begin{aligned} \text{mesure 1} \\ \text{tension (1)} &= 10.19 \text{ mV} \\ \text{tension (2)} &= 25.8 \text{ mV} \\ \text{tension (3)} &= 48.55 \text{ mV} \\ \text{tension (4)} &= 52.2 \text{ mV} \\ \text{tension (5)} &= 57.36 \text{ mV} = 1.4 \text{ V} \end{aligned} \right\} \gamma_{el} = 3,45 \mu\text{s}$$

$$\left. \begin{aligned} \text{mesure 2} \\ \text{tension (1)} &= 10.20 \text{ mV} \\ \text{tension (2)} &= 25.8 \text{ mV} \\ \text{tension (3)} &= 48.55 \text{ mV} \\ \text{tension (4)} &= 52.2 \text{ mV} \\ \text{tension (5)} &= 57.36 \text{ mV} = 1.4 \text{ V} \end{aligned} \right\} \gamma_{el} = 3,45 \mu\text{s}$$

mesure 3 :
 tension (1) : 10.19 mV (A)

mesure 4 :
 tension (1) : 10.19 mV (A)

□

$$\left. \begin{aligned} \text{mesure 1} \\ \text{tension (1)} &= 10.19 \text{ mV} \\ \text{tension (2)} &= 25.8 \text{ mV} \\ \text{tension (3)} &= 48.55 \text{ mV} \\ \text{tension (4)} &= 52.2 \text{ mV} \\ \text{tension (5)} &= 57.36 \text{ mV} = 1.4 \text{ V} \end{aligned} \right\} \gamma_{el} = 3,45 \mu\text{s}$$

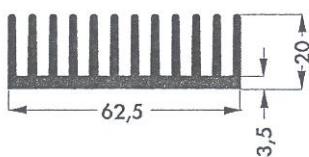
$$\left. \begin{aligned} \text{mesure 2} \\ \text{tension (1)} &= 10.20 \text{ mV} \\ \text{tension (2)} &= 25.8 \text{ mV} \\ \text{tension (3)} &= 48.55 \text{ mV} \\ \text{tension (4)} &= 52.2 \text{ mV} \\ \text{tension (5)} &= 57.36 \text{ mV} = 1.4 \text{ V} \end{aligned} \right\} \gamma_{el} = 3,45 \mu\text{s}$$



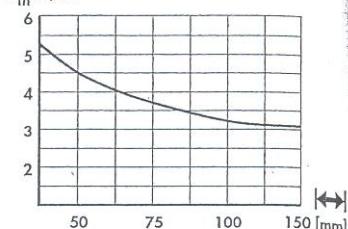
Dissipateurs extrudés standard

art. n°

SK 444 ...



R_{th} [K/W]



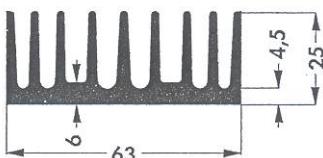
veuillez indiquer:



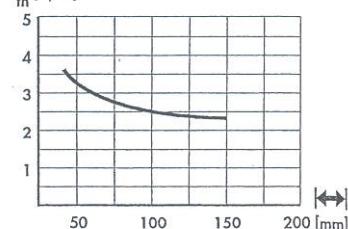
37,5 50 75 1000 mm

art. n°

SK 406 ...



R_{th} [K/W]



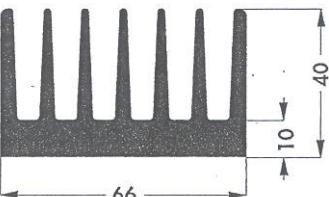
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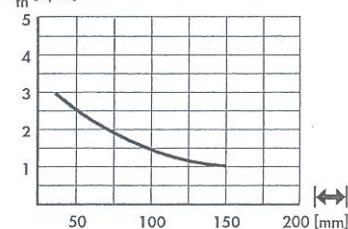
37,5 50 75 100 1000 mm

art. n°

SK 100 ...



R_{th} [K/W]



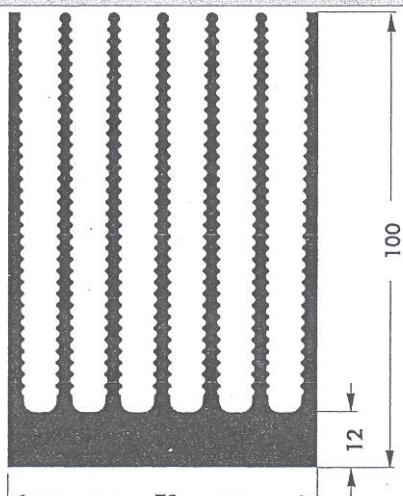
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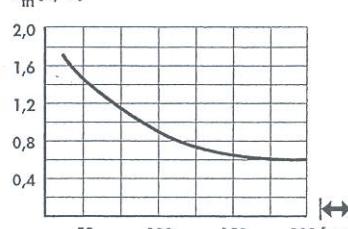
37,5 50 75 100 150 1000 mm

art. n°

SK 506 ...



R_{th} [K/W]



veuillez indiquer:



37,5 50 75 100 1000 mm

... (optional)

SSR 1

Introduction technique

Résistances thermiques des profilés quelconques en convection forcée

$$R_{thKf} \approx a \times R_{thK}$$

R_{thKf} = résistance thermique en convection forcée

R_{thK} = résistance thermique en convection naturelle

a = facteur de proportion

remarques:

1. Les valeurs indiquées dans les diagrammes sont valables pour des dissipateurs anodisés noir et montés verticalement et naturelle convection.

Facteurs de correction: surface naturelle: + 10 bis 15 % et pour montage horizontal: + 15 bis 20 %

2. Les profilés extrudés sont fabriqués selon la norme DIN EN 12020 (ancienne norme DIN 17615 concernant les profilés de précision pour les profilés s'inscrivant dans un cercle supérieur à 300 mm leur tolérance de fabrication correspond à la norme DIN EN 755 (ancienne norme DIN 1748)).

remarque importante:

Pour quelques composants électroniques spéciaux, particulièrement pour les modules avec une grande surface, les IGBT etc., les fabricants des composants stipulent des exigences spécifiques concernant la planéité de la surface de montage des dissipateurs etc., qui sont plus rigides que les tolérances standard. Pour répondre à ces exigences, cette planéité peut seulement être achevée par un fraîrage des surfaces de montage. En plus, il doit également être considéré qu'il peut être nécessaire d'utiliser de jeux de taraudages en fil (Heli-Coil etc) pour achever un couple d'attraction plus haut. Considérez également les remarques des fabricants des semi-conducteurs.

3. Les canaux taraudés extrudés ne sont pas de taraudages selon la norme, car ils ne contiennent pas de montée de taraudage. La montée est seulement simulée à l'aide des nervures (ailettes) en quinconce. L'utilisateur est responsable d'une application appropriée du produit.

4. L'usinage de nos dissipateurs est conforme à la norme DIN ISO 2768 m sauf indications contraires.

5. Les longueurs des profilés extrudés [↔] ainsi que les perforations [●] données dans ce catalogue sont celles de nos standards. Nous réalisons à partir de plan ou d'échantillon des dissipateurs sur mesure. La modernité de notre parc de machines CNC, nous permet de réaliser des alésages, des perçages/ taraudages en opérations simul-tanées (jusqu'à 26 à la fois), des fraisages et des estampages. De ce fait nos prix sont compétitifs et nos délais des plus réduits. Nous sommes à même de réaliser le produit qui résoudra votre problème de refroidissement. La modernité de notre parc de machines CNC, nous permet de réaliser des alésages, des perçages/taraudages en opérations simul-tanées (jusqu'à 26 à la fois), des fraisages et des estampages. De ce fait nos prix sont compétitifs et nos délais des plus réduits. Nous sommes à même de réaliser le produit qui résoudra votre problème de refroidissement.

6. De série nos dissipateurs sont fabriqués dans un aluminium type EN AW 6060 - T66, trempé à chaud (ancienne type AlMgSi05 - F22 à la norme DIN 1748). Les produits standard sont livrés en aluminium brut dégraissé (Version AL), anodisé noir (Version SA) ou avec une anodisation incolore (Version ME) et d'autres couleurs d'anodisation plus décoratives sont possibles sur demande.

7. Si dans notre gamme de 240 profilés pour les dissipateurs courants, de 35 profilés pour les petits dissipateurs et parmi nos 40 modèles de dissipateurs "à doigts" vous n'avez pas trouvé le produit qu'il vous faut: il nous est possible de réaliser, selon vos plans, des dissipateurs spéciaux.

8. Tolerances des fabrications.

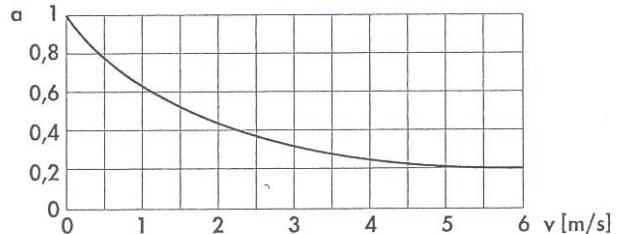
Toutes les dimensions de nos fabrications de notre catalogue et des produits usinés sur demande (sauf précision spéciale) sont conformes à la norme DIN ISO 2768 m. Pour les profilés, les pièces moulées, les poignées et les amortisseurs d'oscillations correspondent à d'autres normes spécifiques.

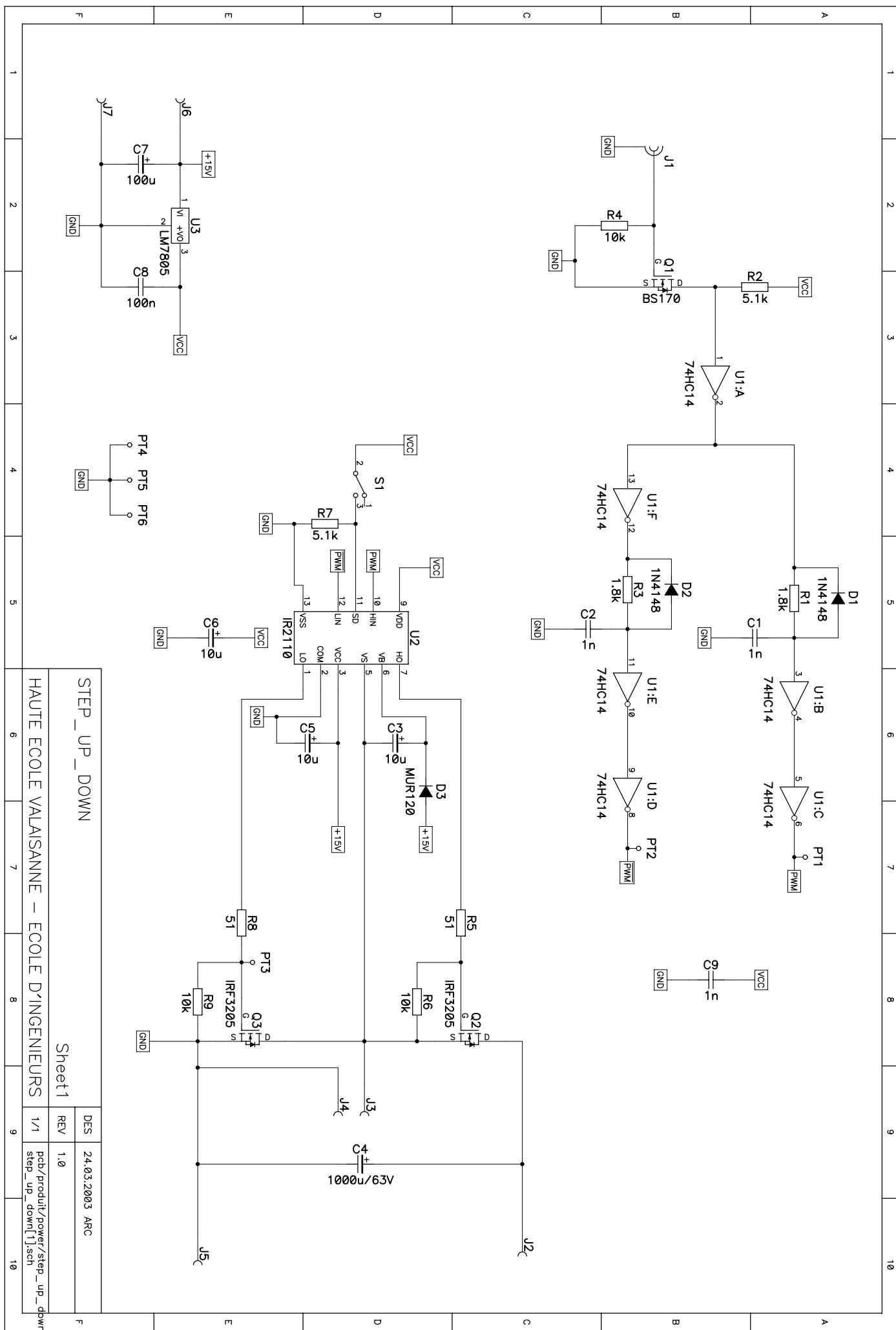
Stand - mai 2006

Nous déclinons toutes responsabilités sur les conséquences que pourraient occasionner d'éventuelles erreurs d'impression.

Nous nous réservons le droit de modifier à tout moment certains aspects et caractéristiques techniques de ces produits dans un constant souci d'amélioration. Tous les produits de ce catalogue qui ne sont pas issus de nos fabrications et bien que ceux-ci ne soient pas mentionnés, conservent les caractéristiques et certifications garanties par leurs fabricants. La reproduction et la photocopie, même partielles, du contenu de ce catalogue sont seulement autorisées en cas d'une autorisation explicite et par écrit de la part de Fischer Elektronik. Toutes les informations données dans ce catalogue, les textes, les dessins, les documents sont soumis au droit d'auteur et à la remarque de protection qui limite l'utilisation de documents et de produits selon DIN ISO 16016. Tous droits réservés.

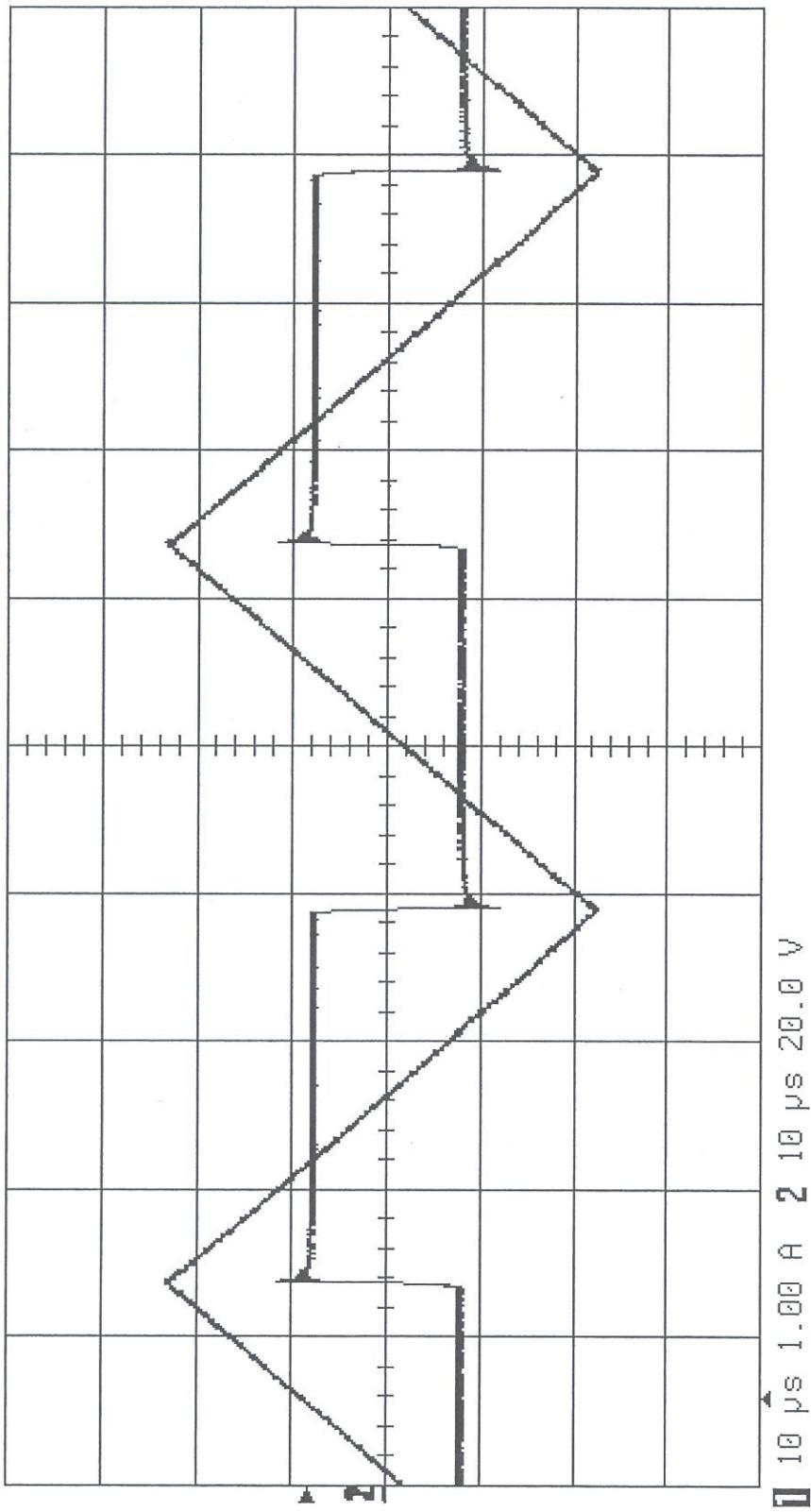
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Mesure de L_1

Annexe 6

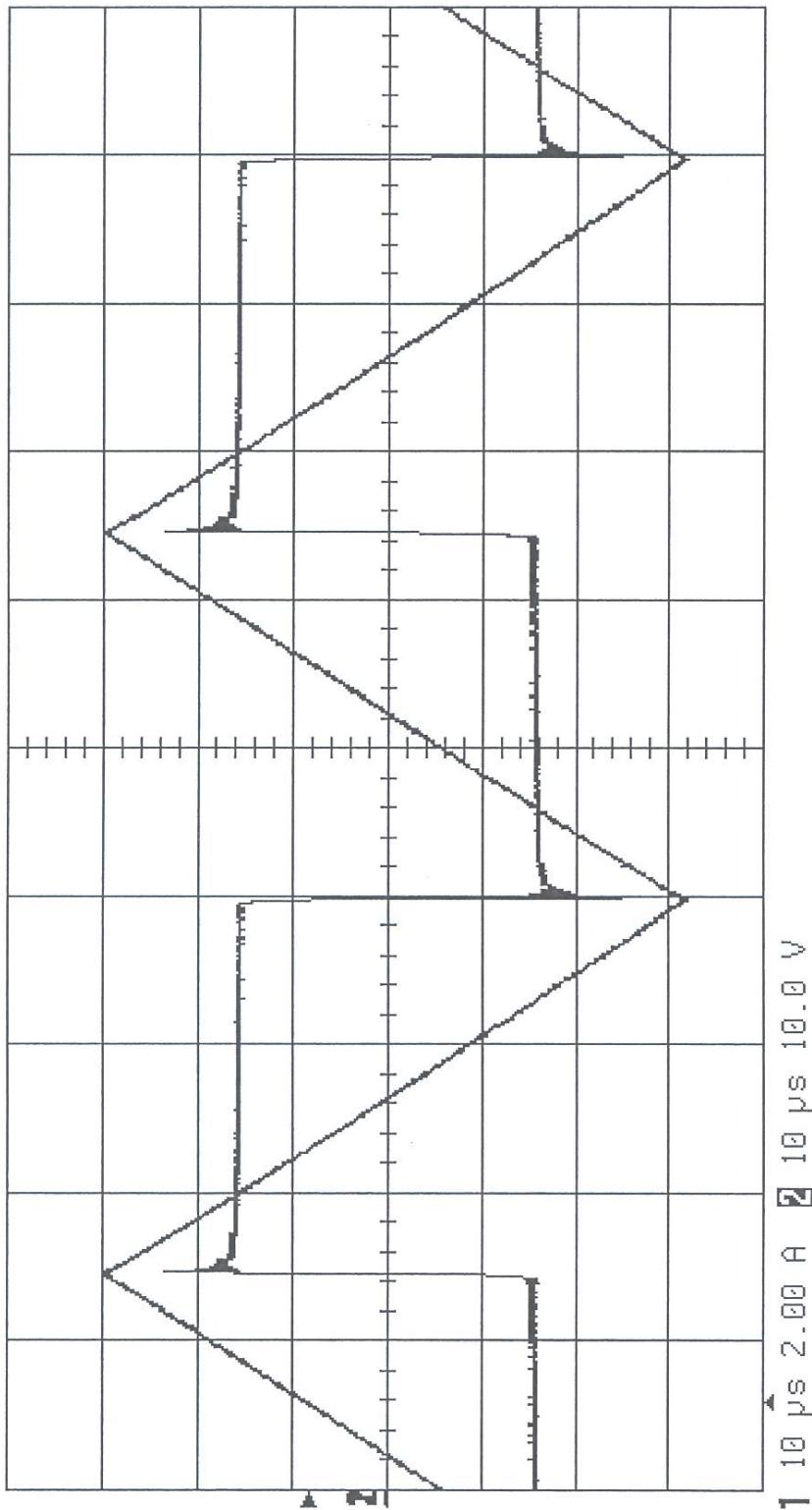


$pk\text{pk}(1) = 4.63 \mu s$
period(1) = 50.0250 μs
rms(2) = 15.91 V

$$\Rightarrow L_1 = U_L \cdot \frac{dt}{di} = 85,95 \mu H$$

STOPPED

Mesure de L_{CC}



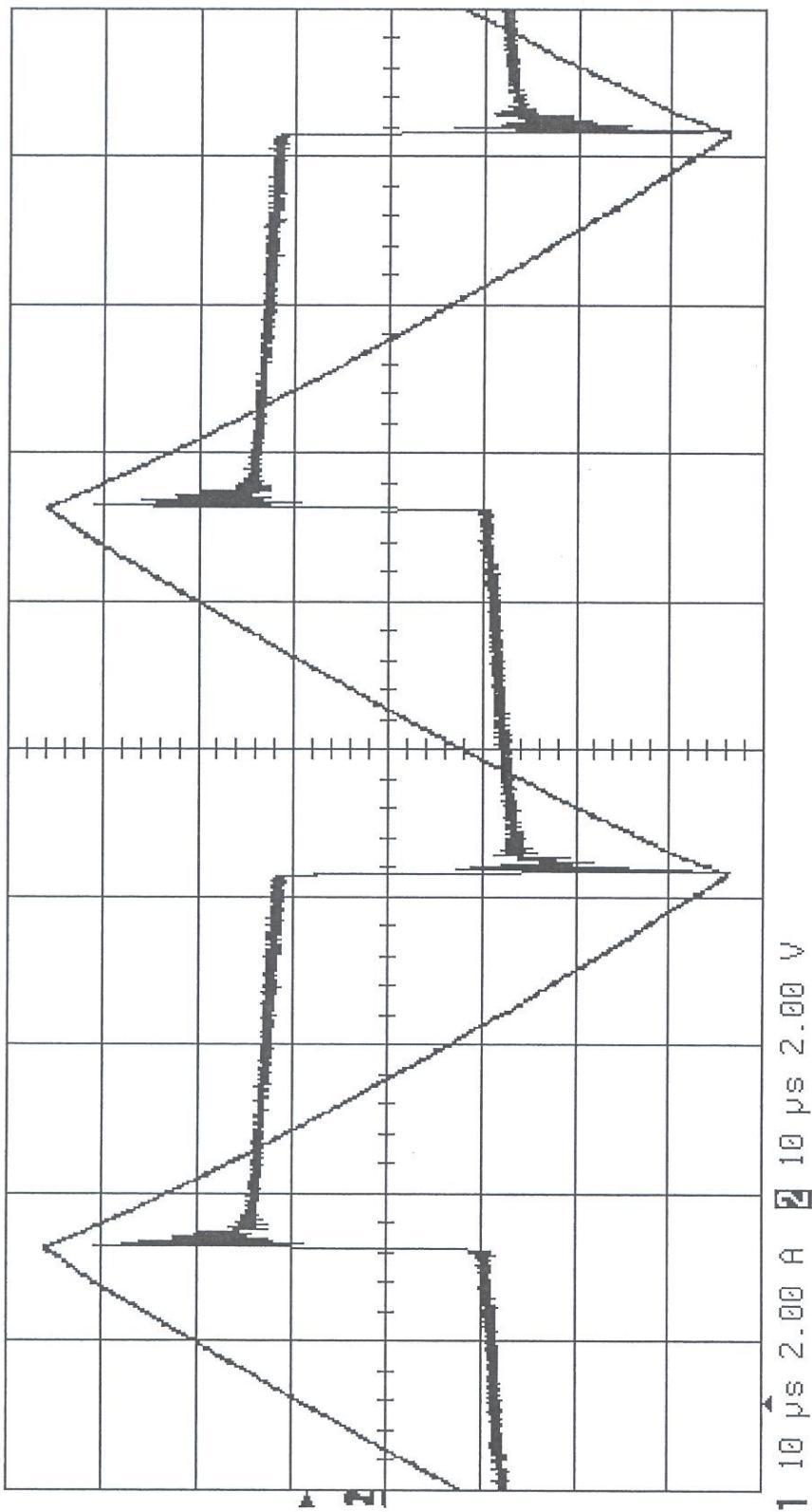
1 10 μ s 2.00 A [2] 10 μ s 10.0 V

pkpk(1) 12.38 A
period(1) 50.0790 μ s
rms(2) 15.72 V

$$L_{CC1} = U_L \cdot \frac{dt}{di} = 31.79 \mu H$$

□ STOPPED

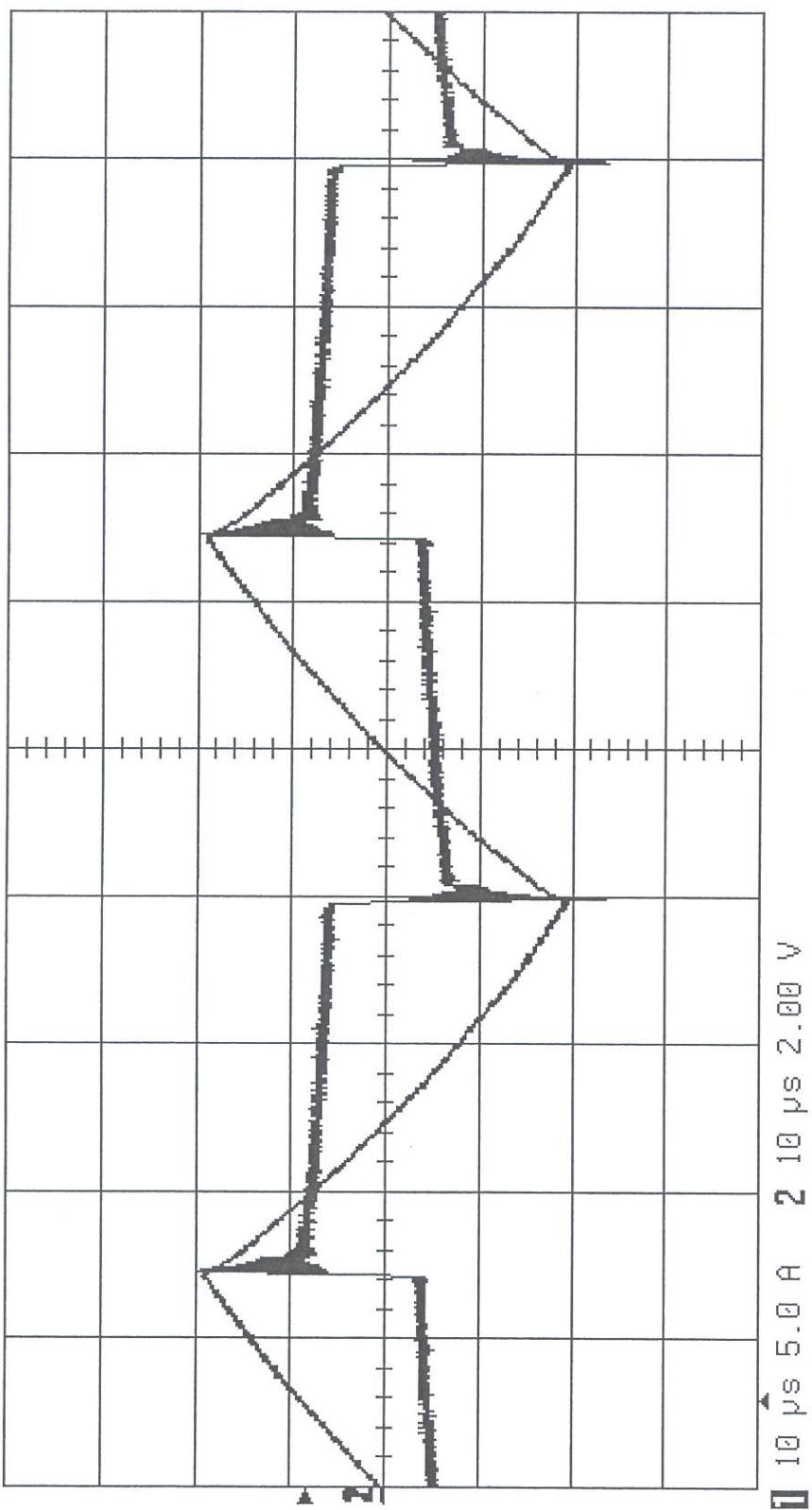
Mesure de L_2



$$\text{pkpk(1)} \quad 14.44 \text{ A} \\ \text{period(1)} \quad 50.0330 \mu\text{s} \\ \text{rms(2)} \quad 2.549 \text{ V}$$
$$\Rightarrow L_2 = U_L \cdot \frac{dt}{dI} = 4,416 \mu\text{H}$$

□ STOPPED

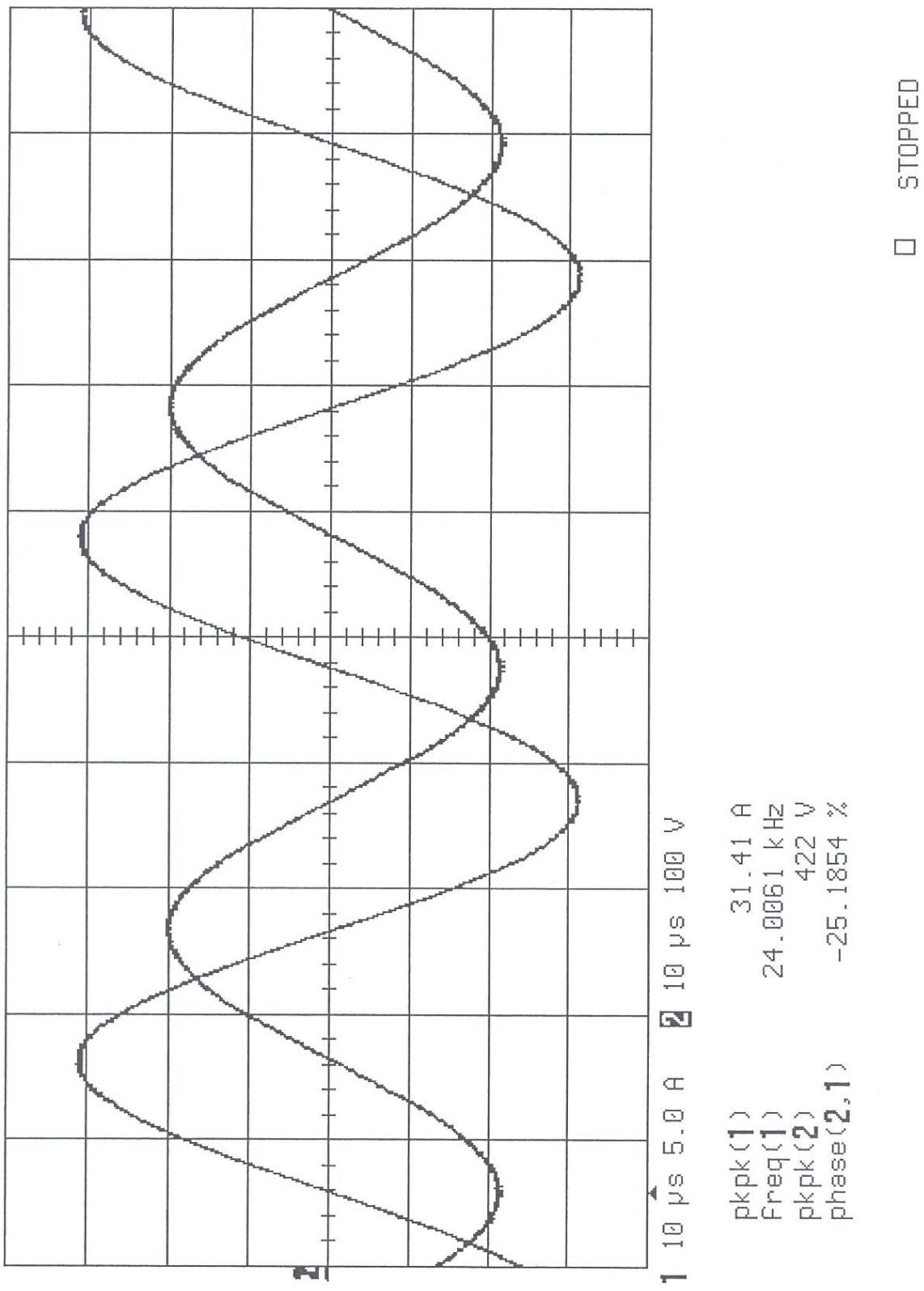
Mesure de L_{CC2}



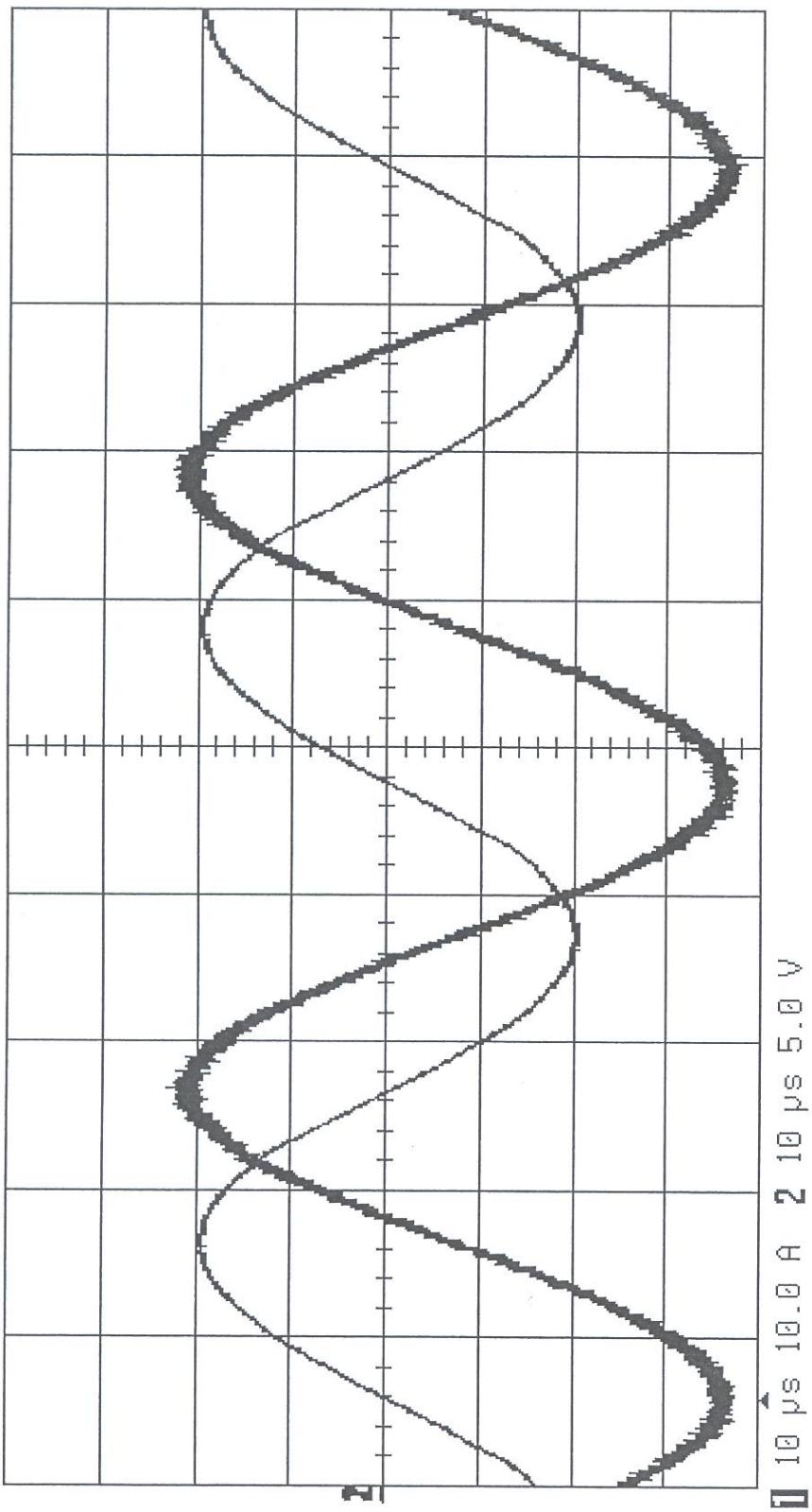
$$\begin{aligned} \text{pkpk (1)} &= 19.53 \text{ A} \\ \text{period (1) } \Rightarrow & 49.9140 \text{ } \mu\text{s} \\ \text{rms (2)} &= 1.296 \text{ V} \end{aligned} \Rightarrow L_{CC2} = U_L \cdot \frac{dt}{di} = 1.65 \mu\text{H}$$

□ STOPPED

Résonance primaire



Résonance secondaire



I 10 μ s 10.0 A 2 10 μ s 5.0 V

pkpk(1) 40.3 A
Freq(1) 23.9943 kHz
pkpk(2) 30.63 V
phase(2,1) -28.9190 %

□ STOPPED

Ferrite ring cores (toroids)

TN23/14/7

RING CORES (TOROIDS)

Effective core parameters

SYMBOL	PARAMETER	VALUE	UNIT
$\Sigma(I/A)$	core factor (C1)	1.81	mm^{-1}
V_e	effective volume	1722	mm^3
l_e	effective length	55.8	mm
A_e	effective area	30.9	mm^2
m	mass of core	≈8.4	g

Coating

The cores are coated with polyamide 11 (PA11), flame retardant in accordance with UL 94V-2.

Isolation voltage: 2000 V. This is measured with a DC voltage. Contacts are applied on the edge of the ring core, which is also the critical point for the winding operation.

Non-coated cores are available on request.

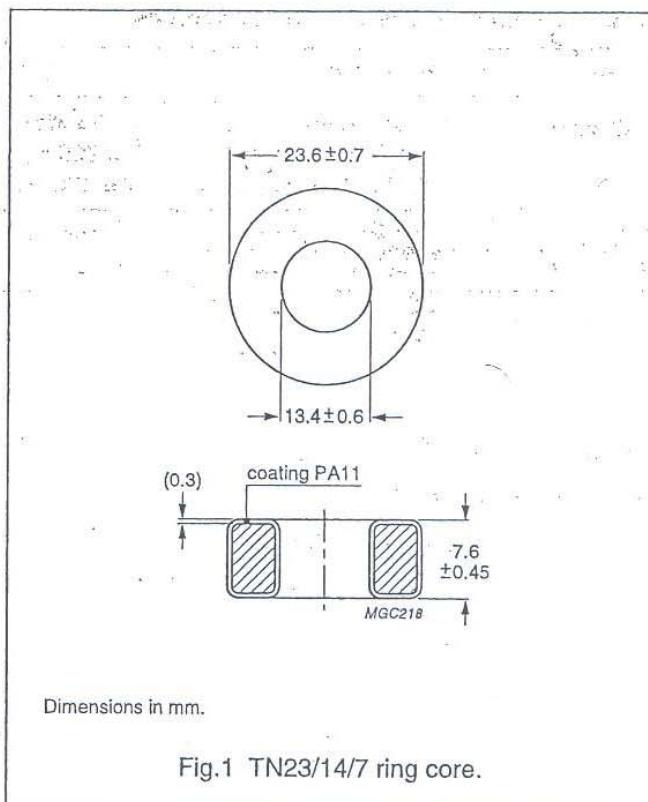


Fig.1 TN23/14/7 ring core.

Ring core data

GRADE	A_L (nH)	μ_i	COLOUR CODE	TYPE NUMBER
4C65	87 ± 25%	≈125	violet	TN23/14/7-4C65
4A11	485 ± 25%	≈700	pink	TN23/14/7-4A11
3R1(1)		≈800	black	TN23/14/7-3R1
3F3	1250 ± 25%	≈1800	blue	TN23/14/7-3F3
3C85	1400 ± 25%	≈2000	red	TN23/14/7-3C85
3C11	3000 ± 25%	≈4300	white	TN23/14/7-3C11
3E25	3820 ± 25%	≈5500	orange	TN23/14/7-3E25

Note

1. Due to the rectangular BH-loop of 3R1, inductance values strongly depend on the magnetic state of the ring core and measuring conditions. Therefore no A_L value is specified. For the application in magnetic amplifiers A_L is not a critical parameter.

Material grade specification

Material grade specification

3

SYMBOL	CONDITIONS	VALUE	UNIT
μ_i	25 °C; ≤10 kHz; 0.1 mT	1800 ±20%	
μ_a	100 °C; 25 kHz; 200 mT	≈4000	
B	25 °C; 10 kHz; 250 A/m	≥2400	mT
	100 °C; 10 kHz; 250 A/m	≥330	
P_V	100 °C; 100 kHz; 100 mT	≤80	kW/m ³
	100 °C; 400 kHz; 50 mT	≤150	
ρ	DC, 25 °C	≈2	Ωm
T_C		≥2200	°C
density		≈4750	kg/m ³

Fig.1 Complex permeability as a function of frequency.

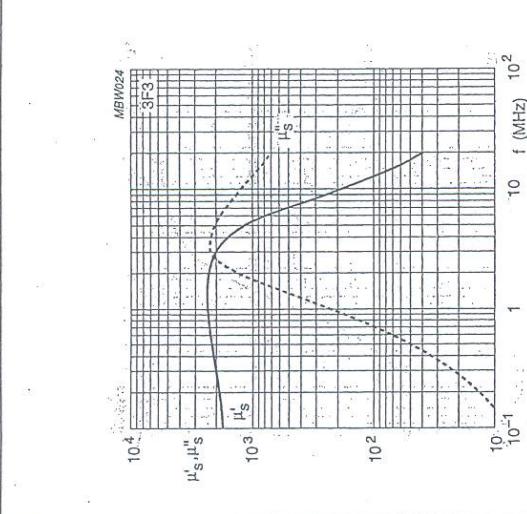


Fig.4 Amplitude permeability as function of peak flux density.

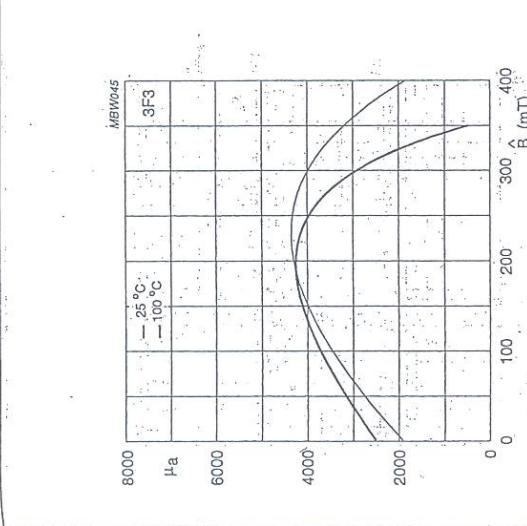


Fig.5 Incremental permeability as a function of magnetic field strength.

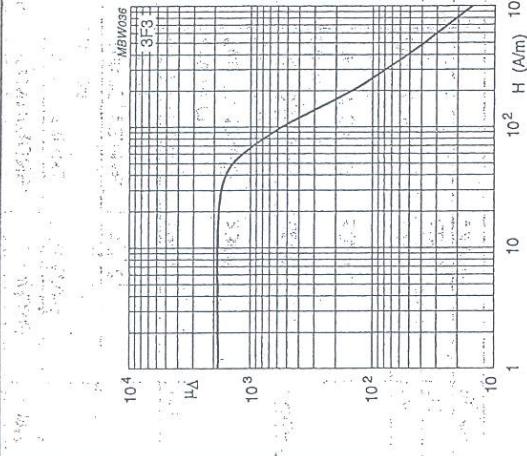
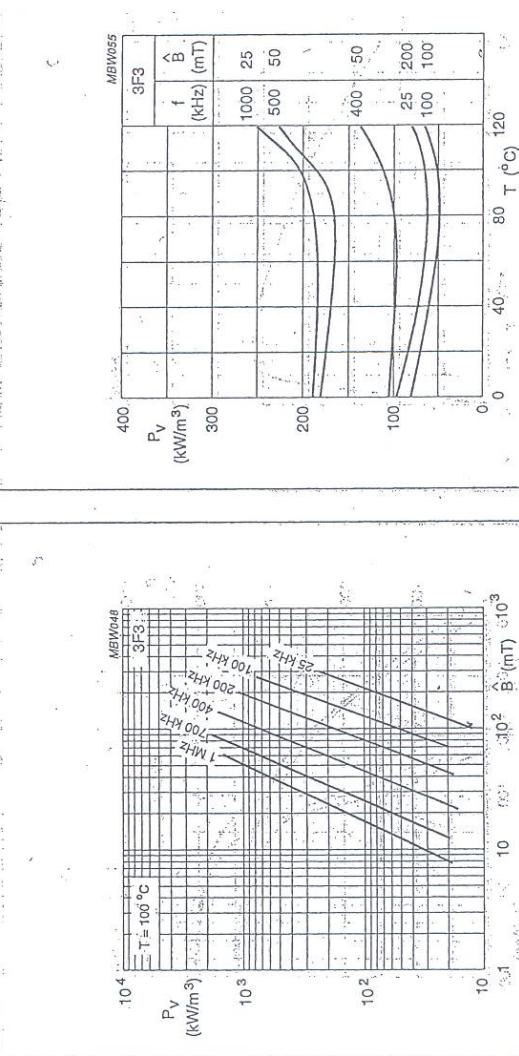
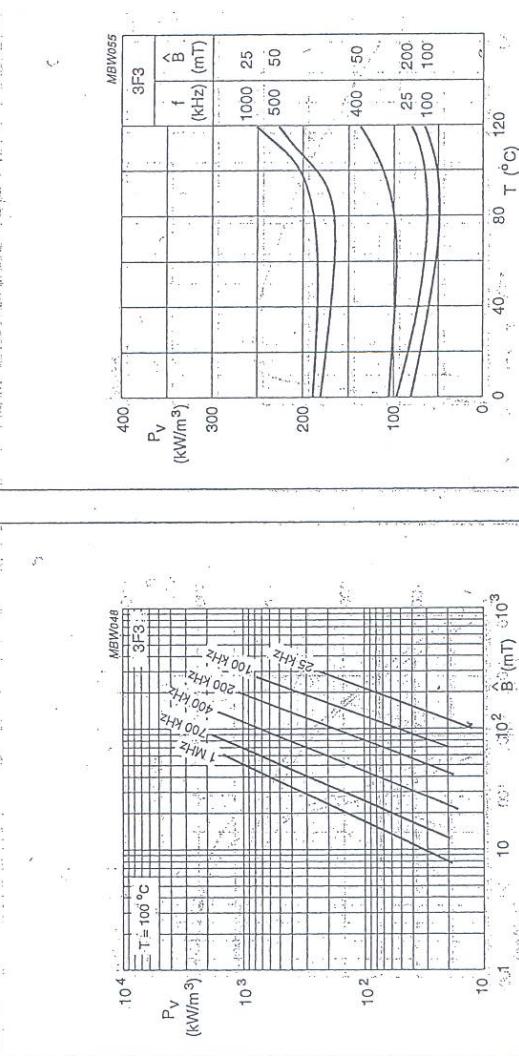
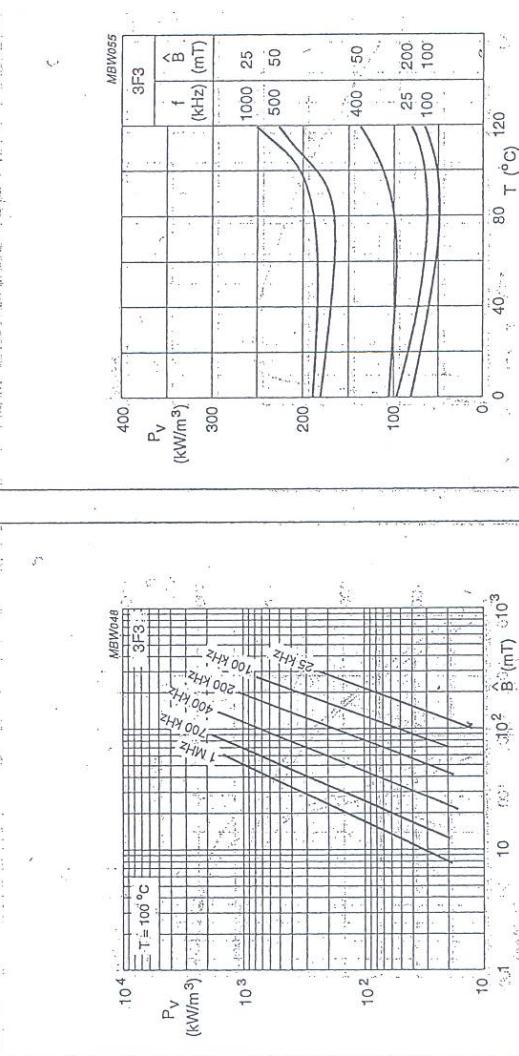
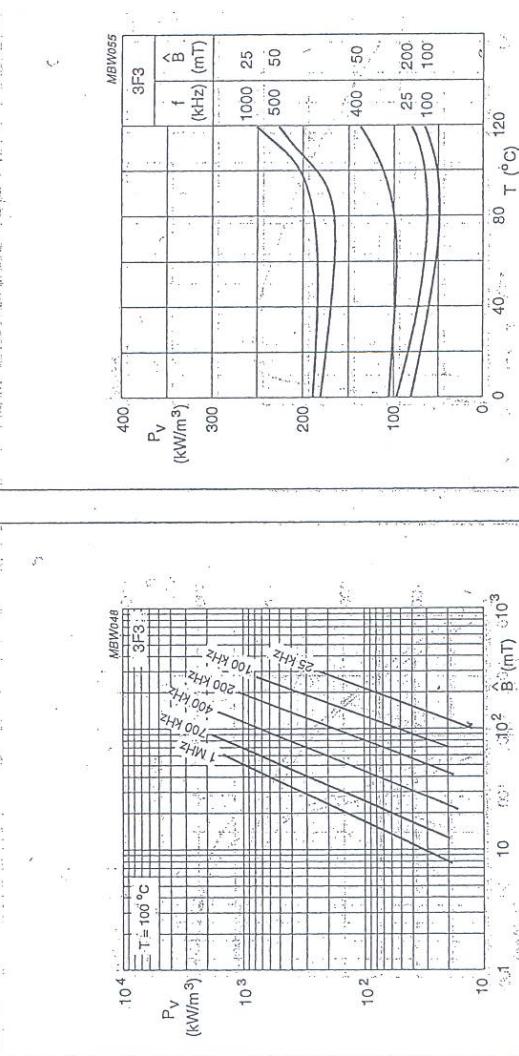
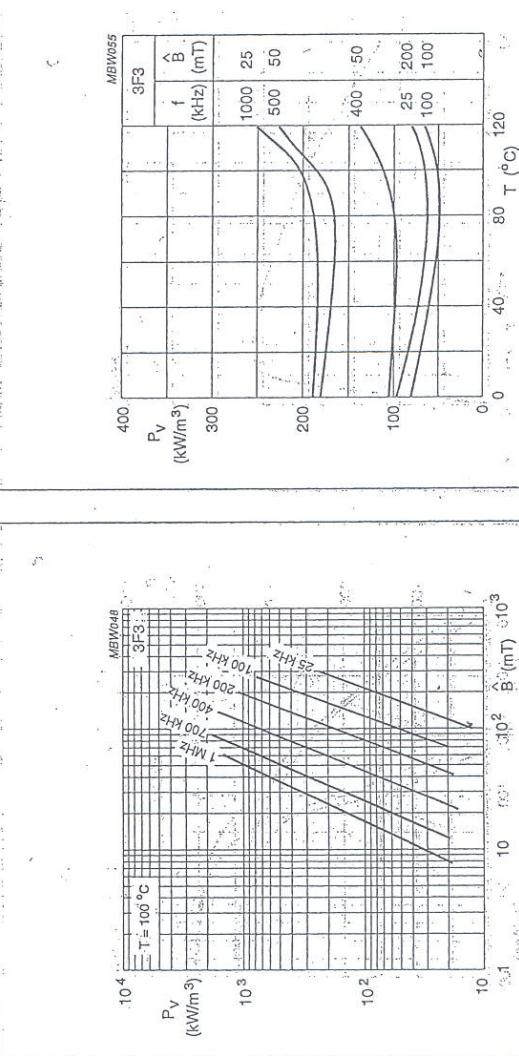
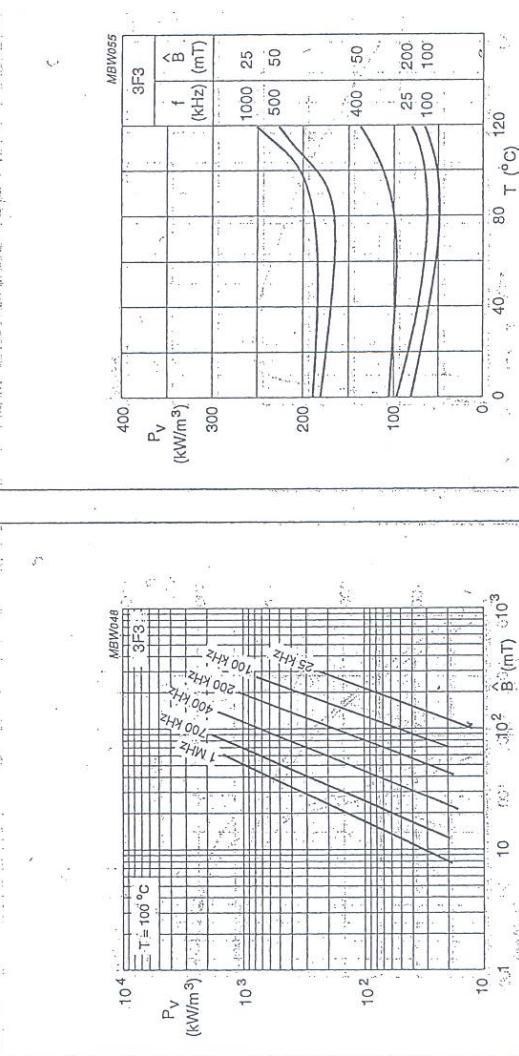
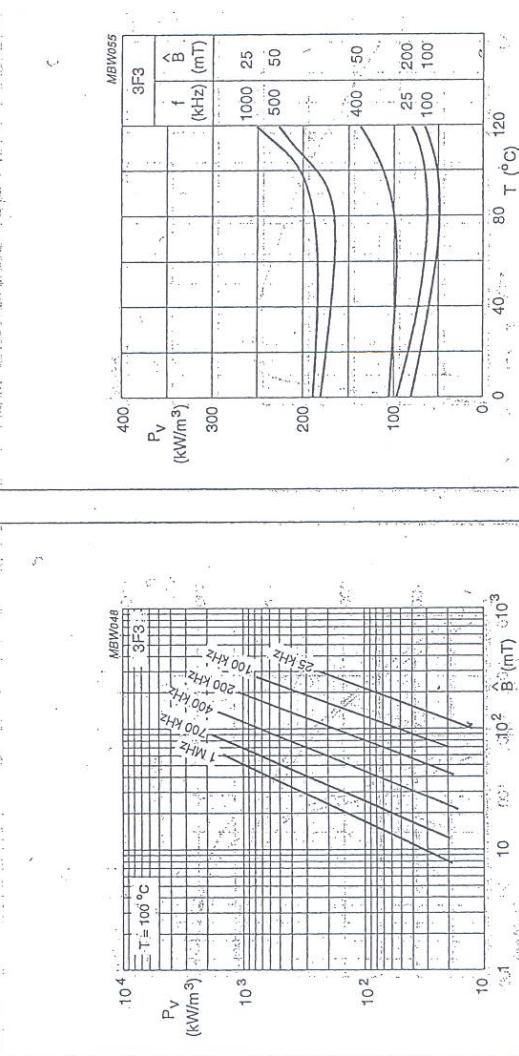
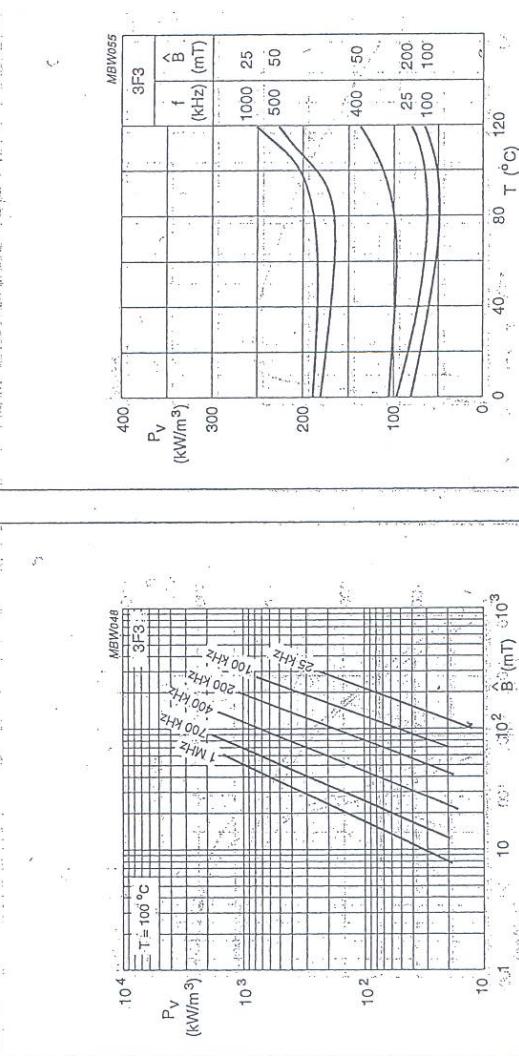
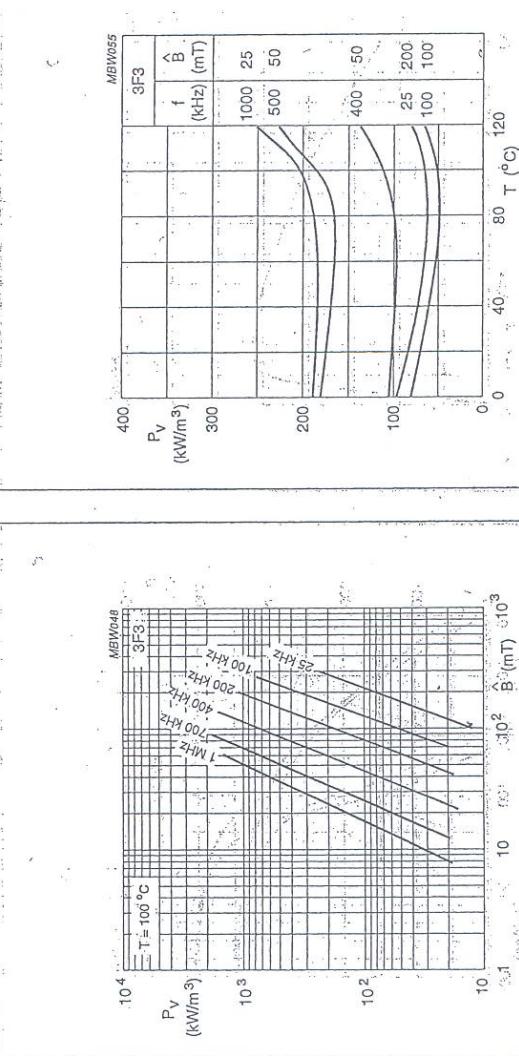
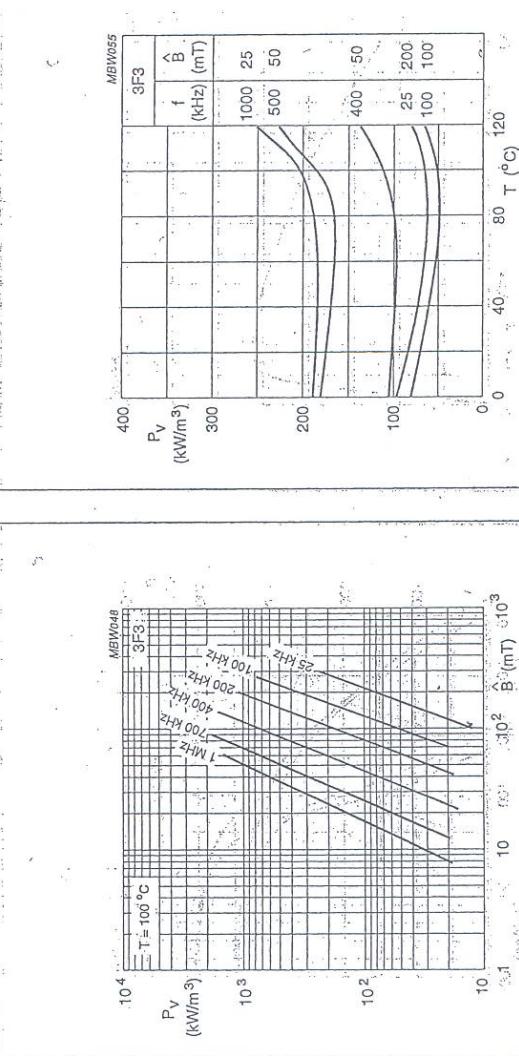
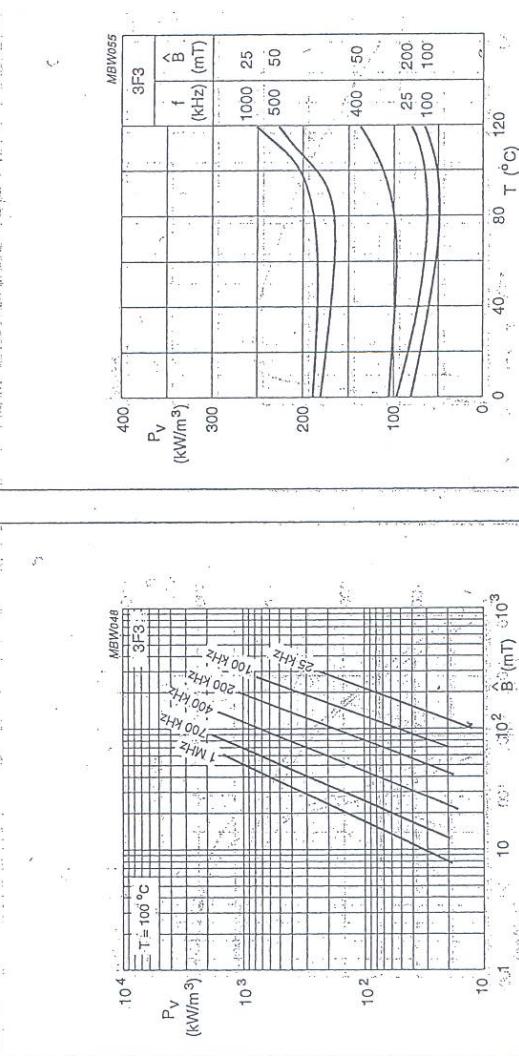
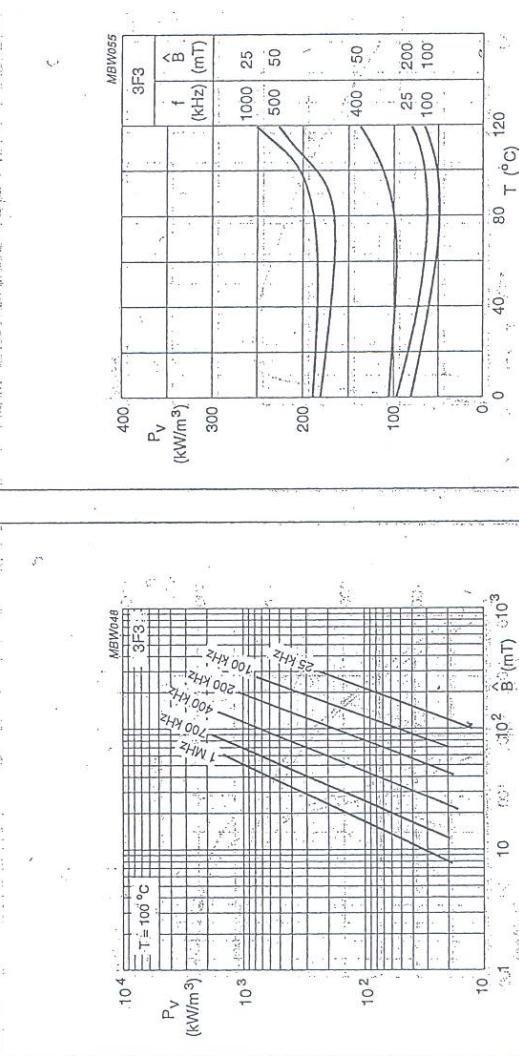
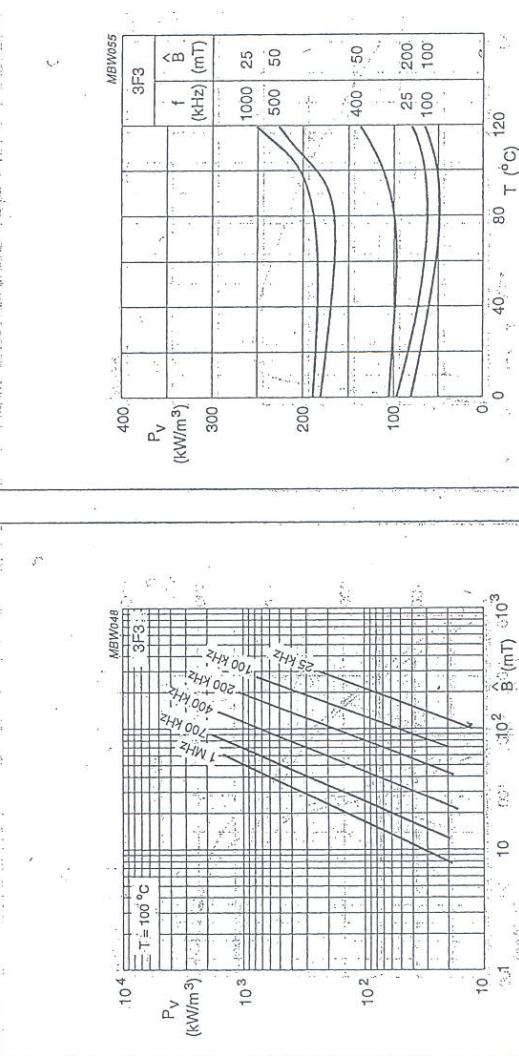
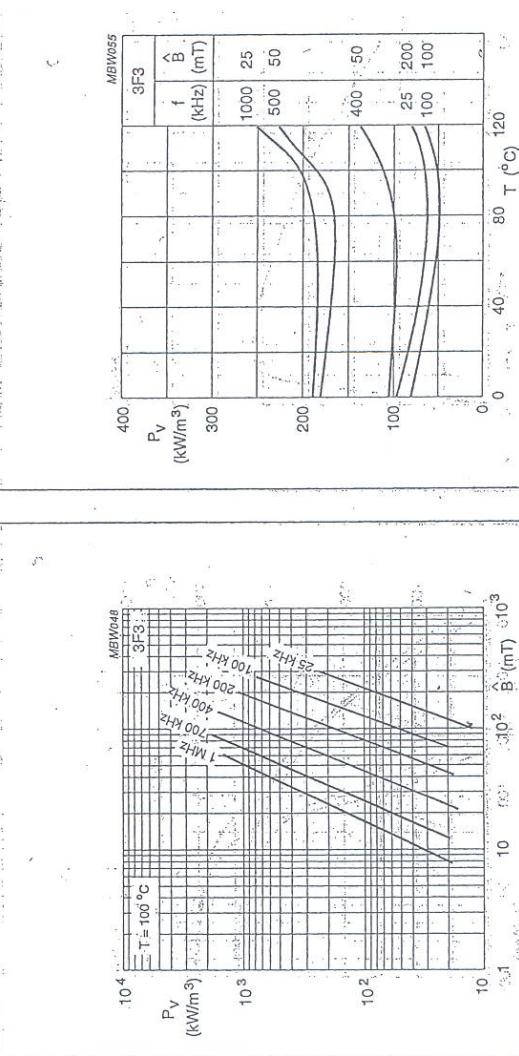
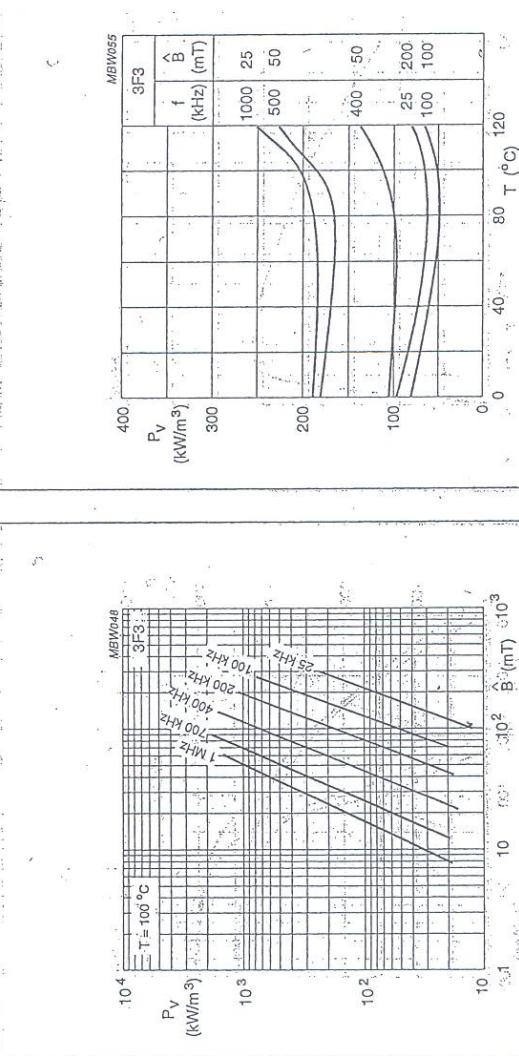
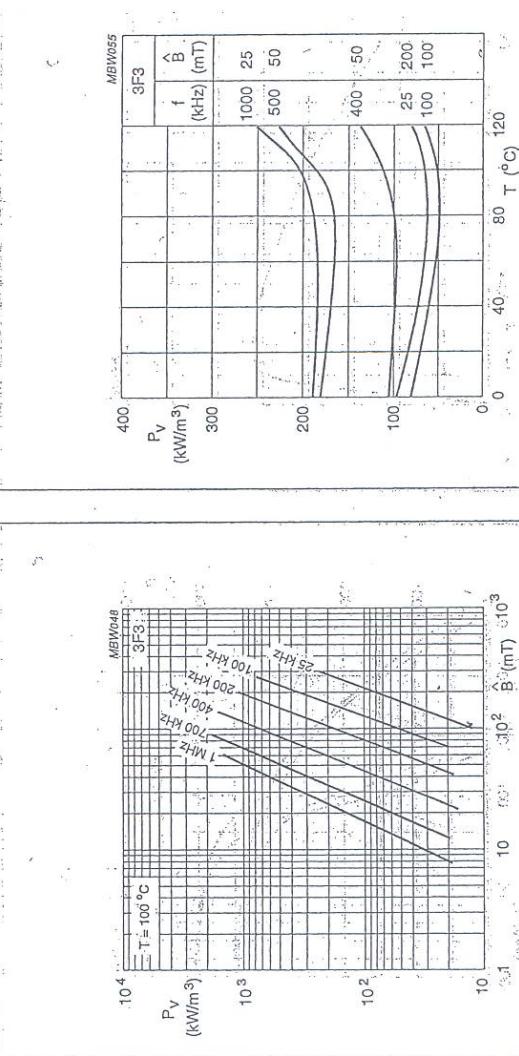
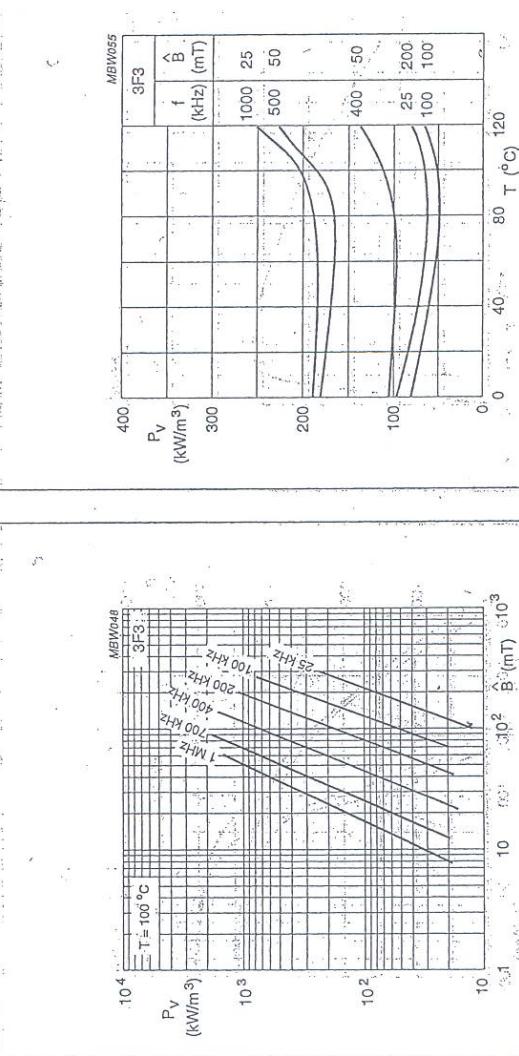
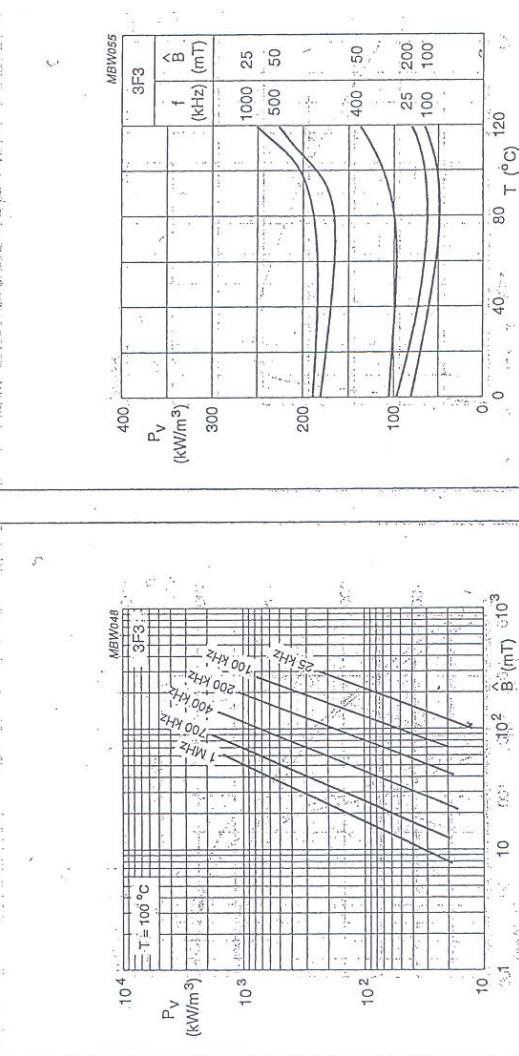
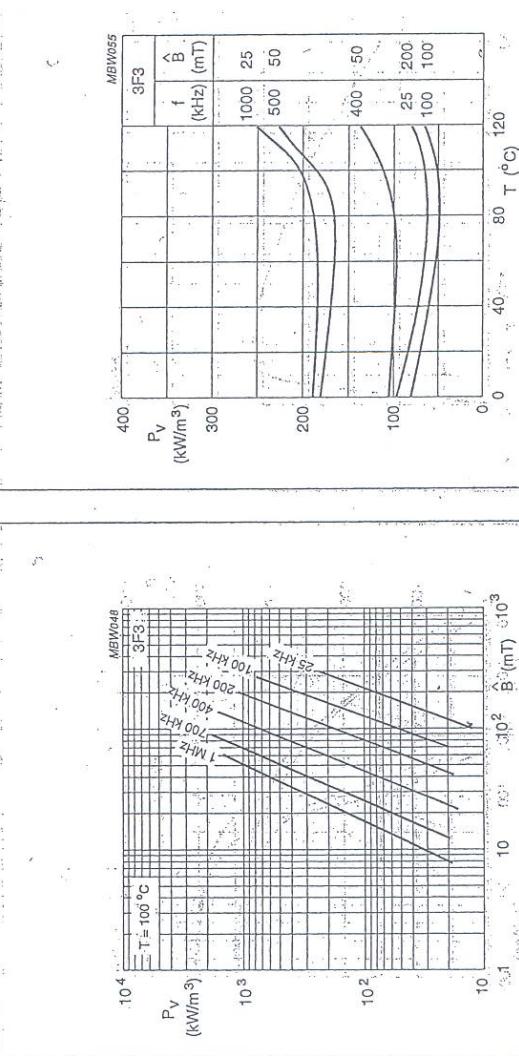
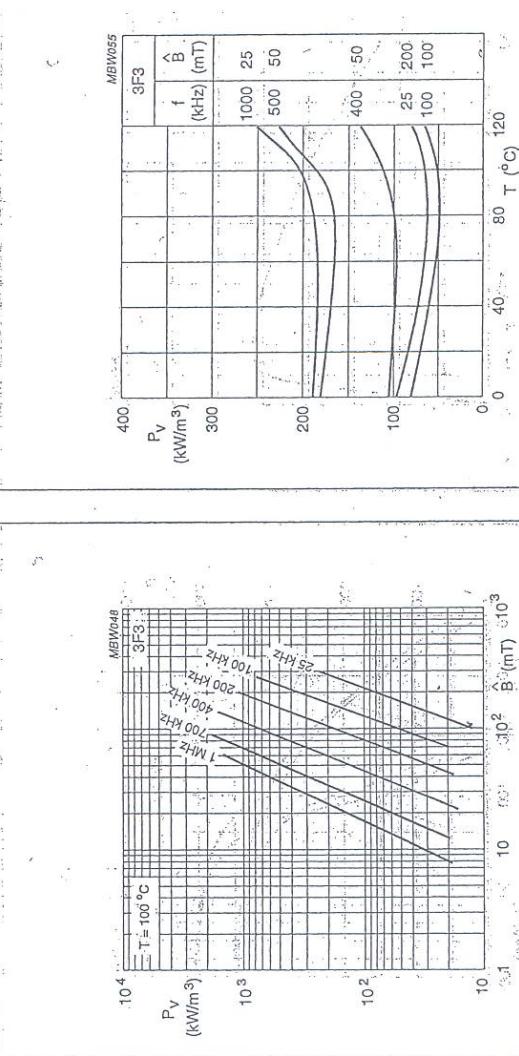
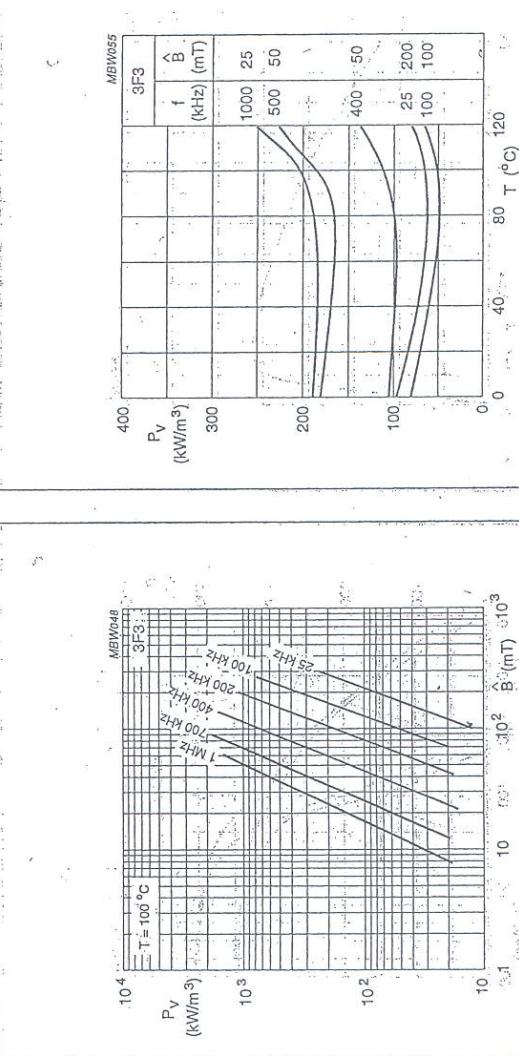
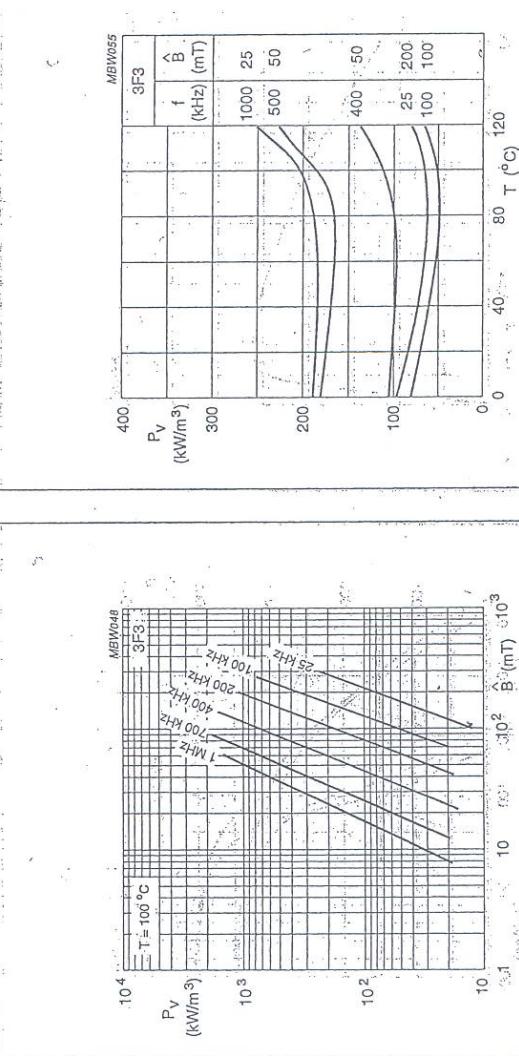
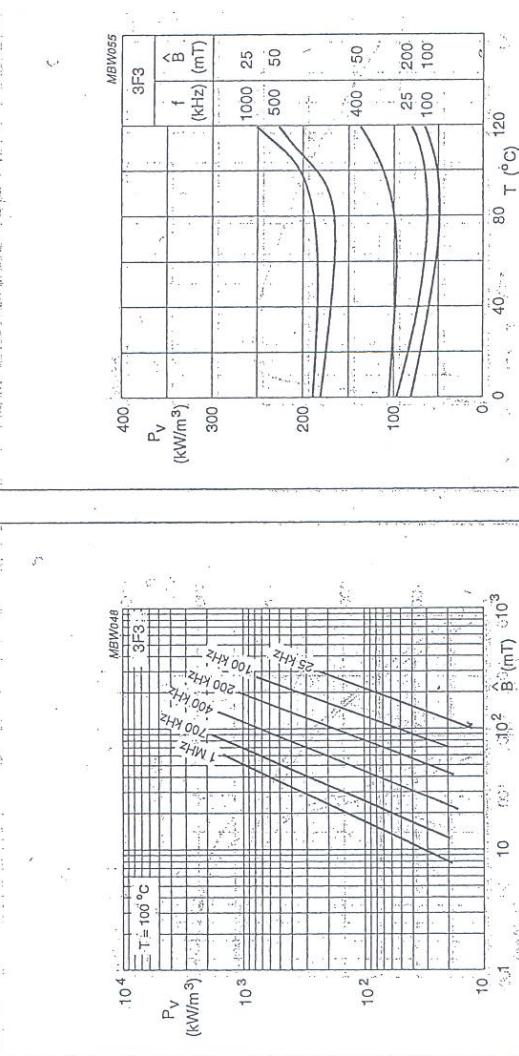
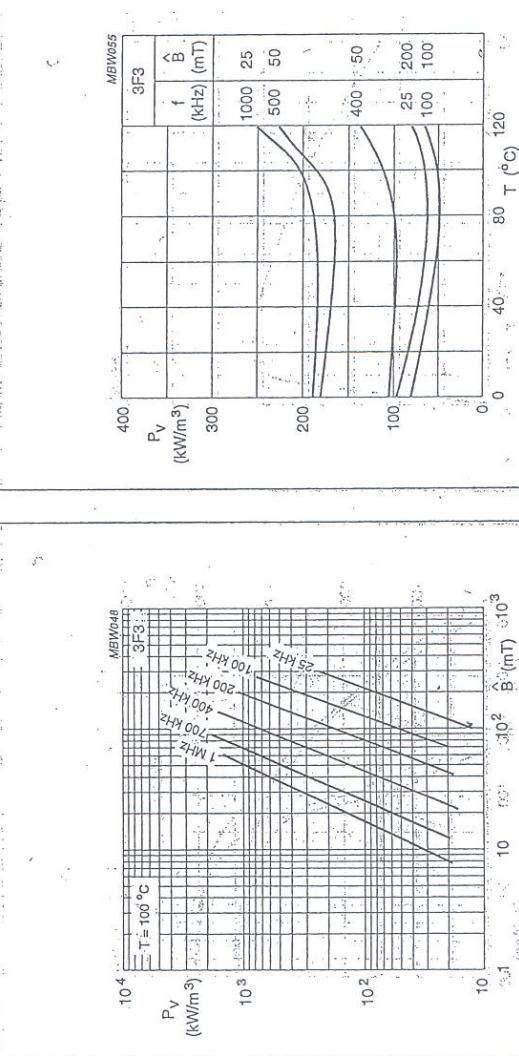
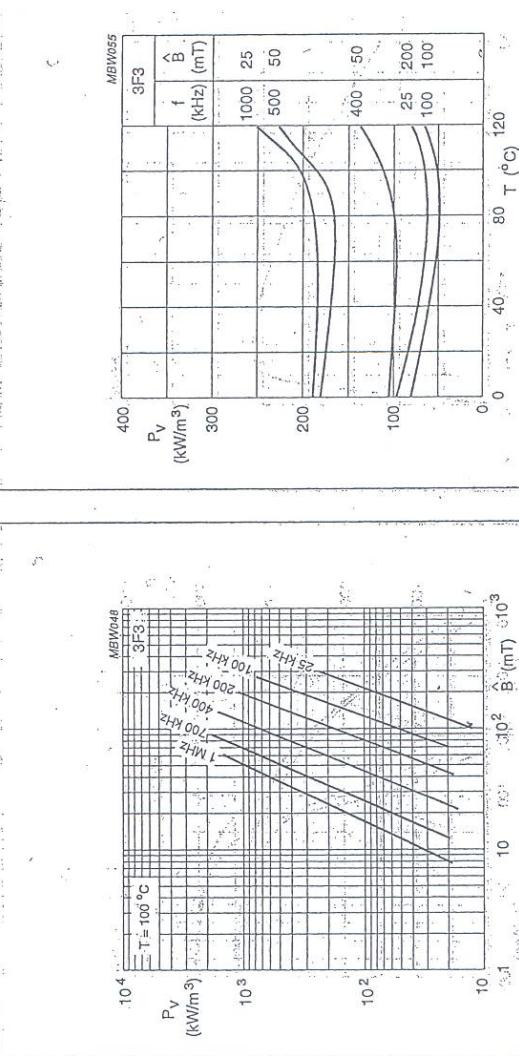
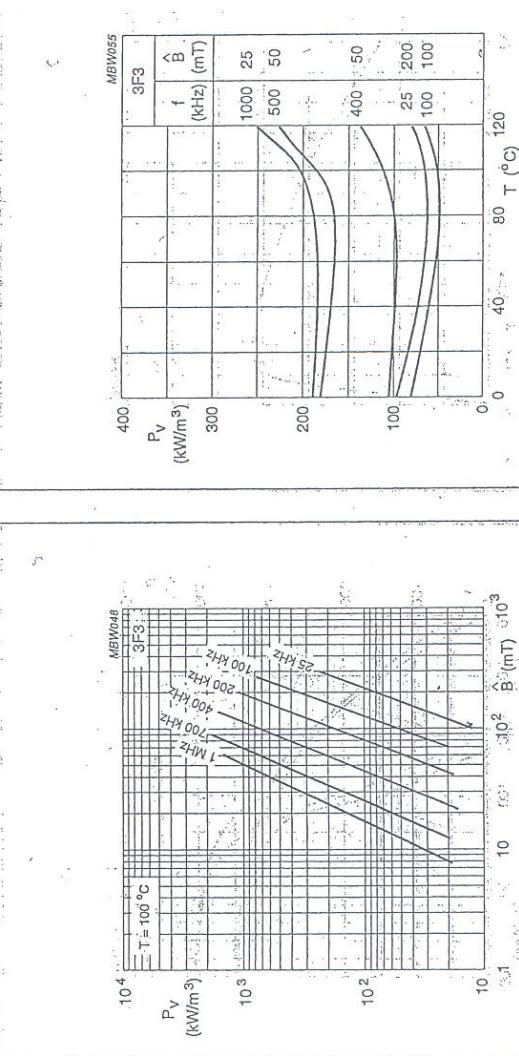
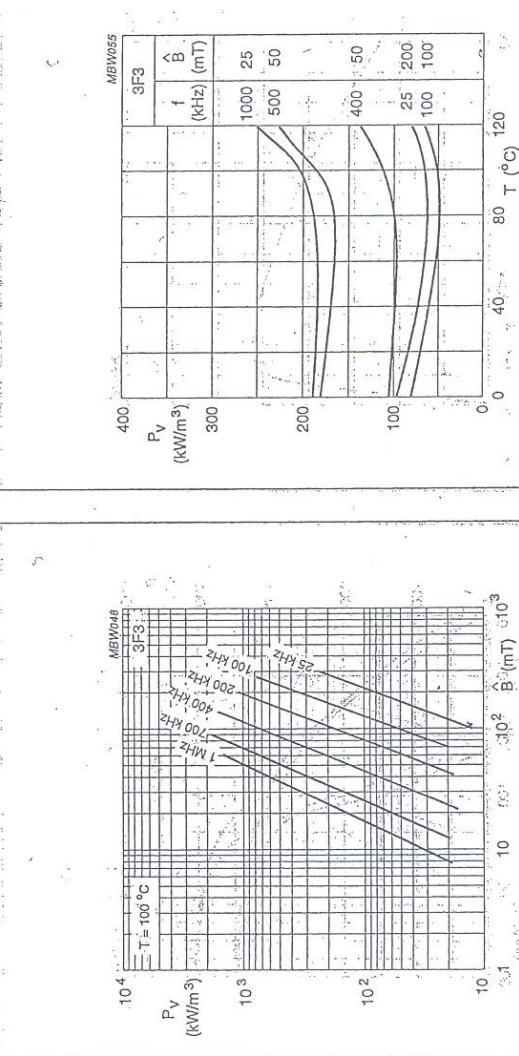
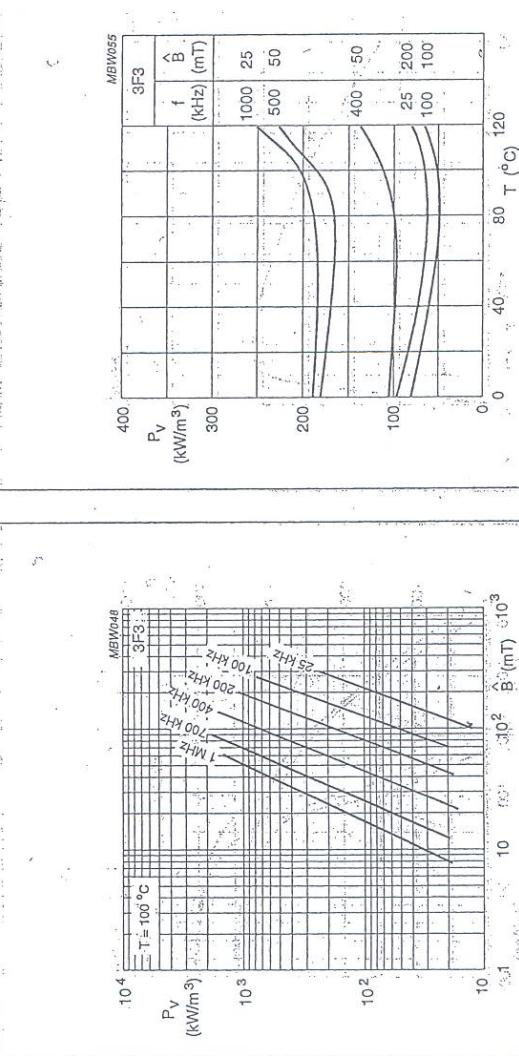
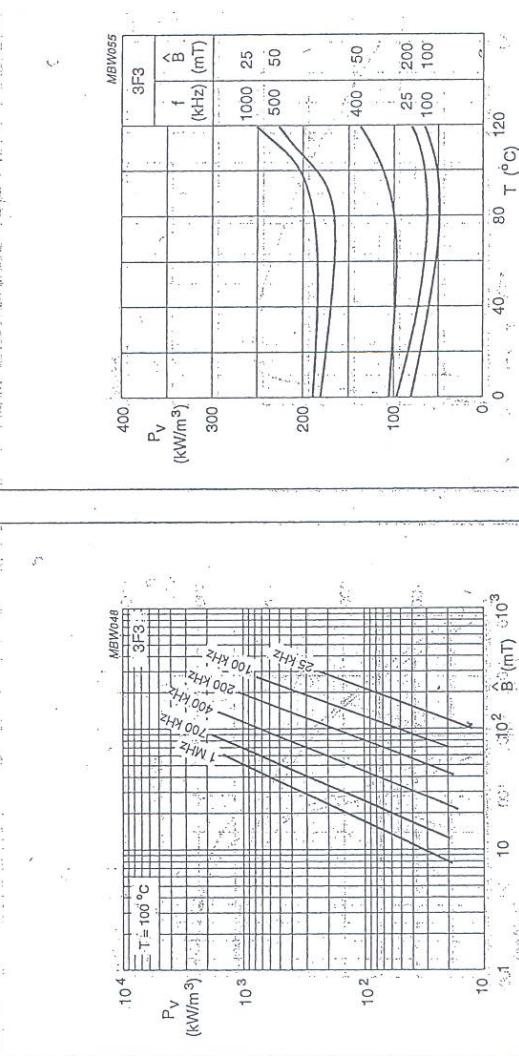
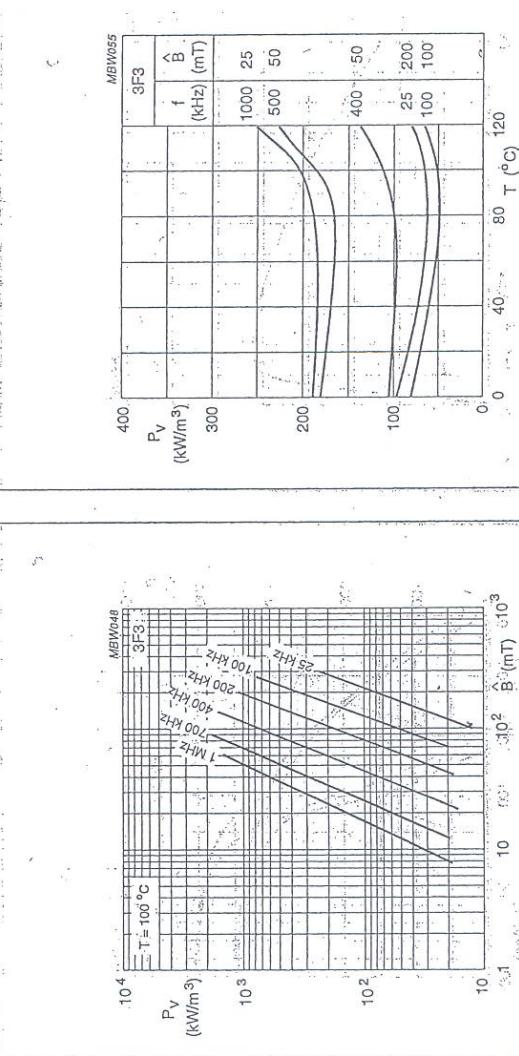
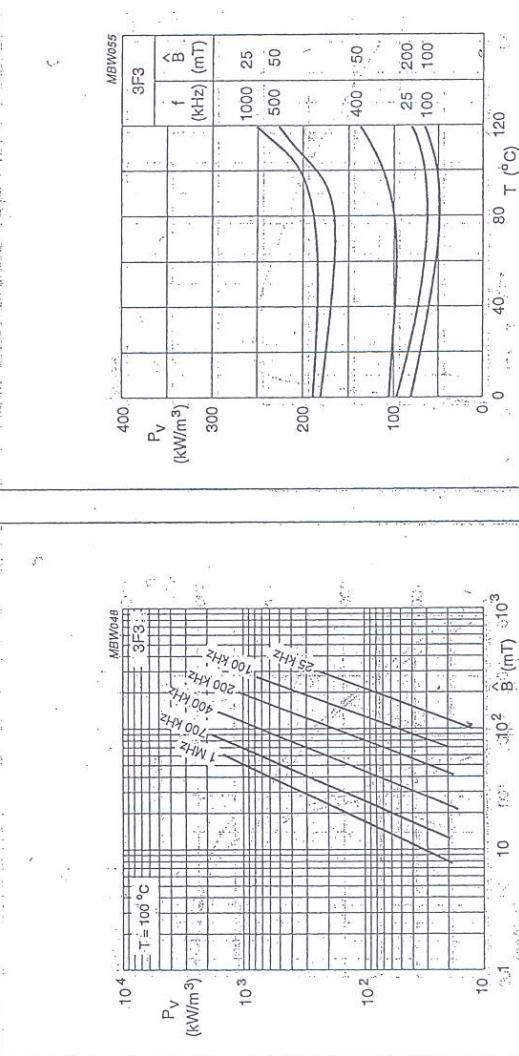
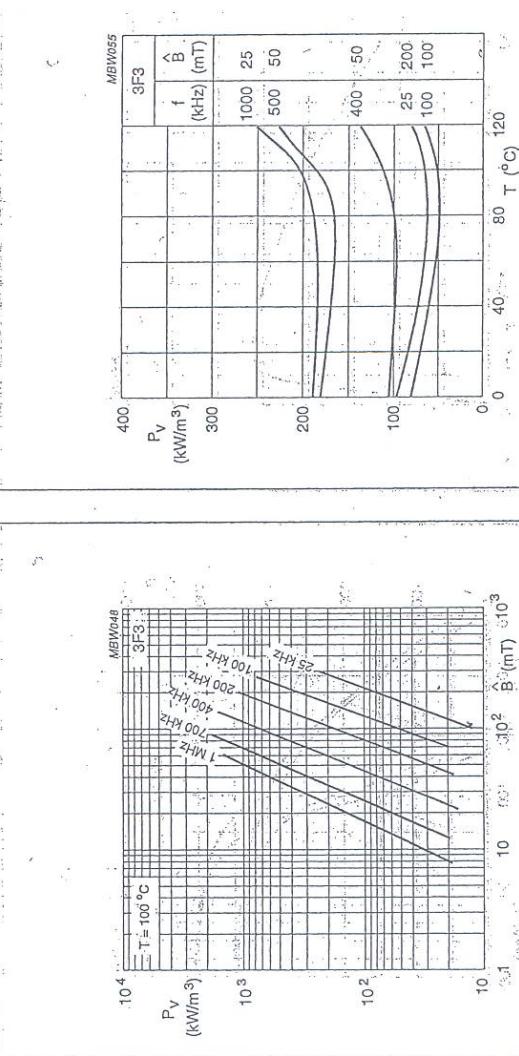
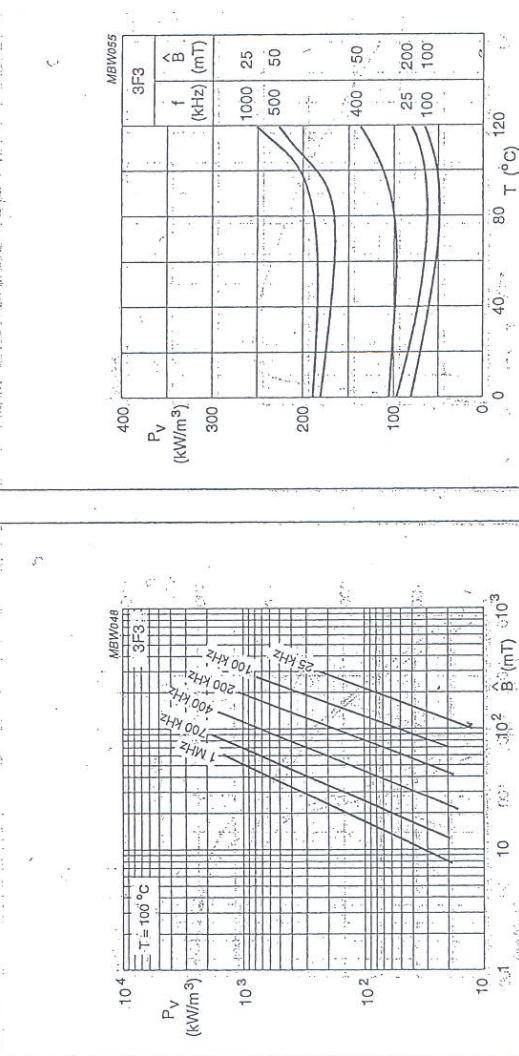
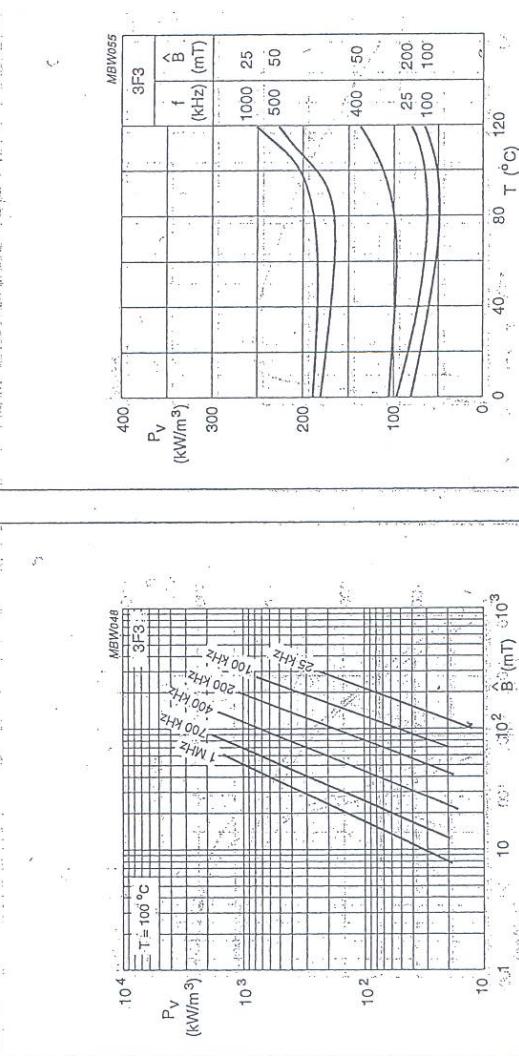
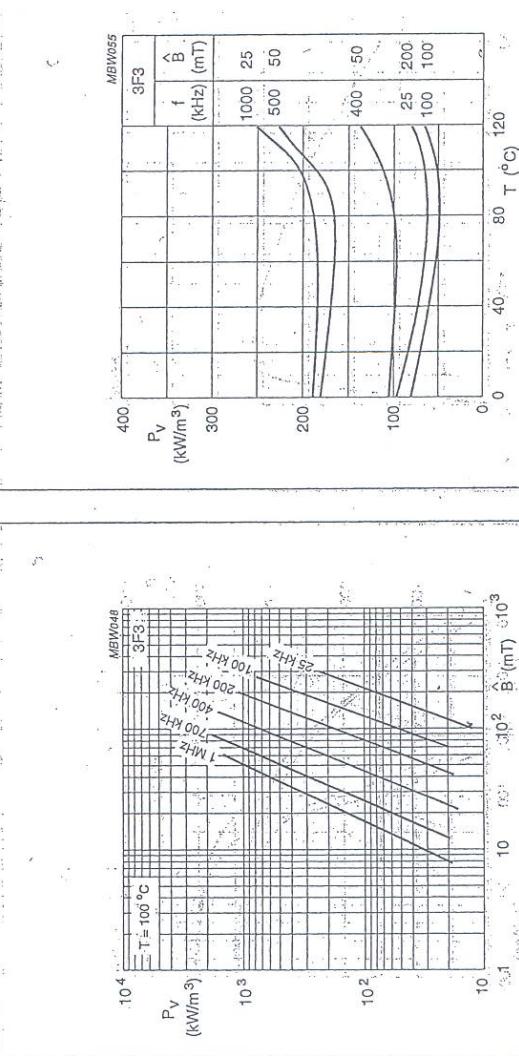
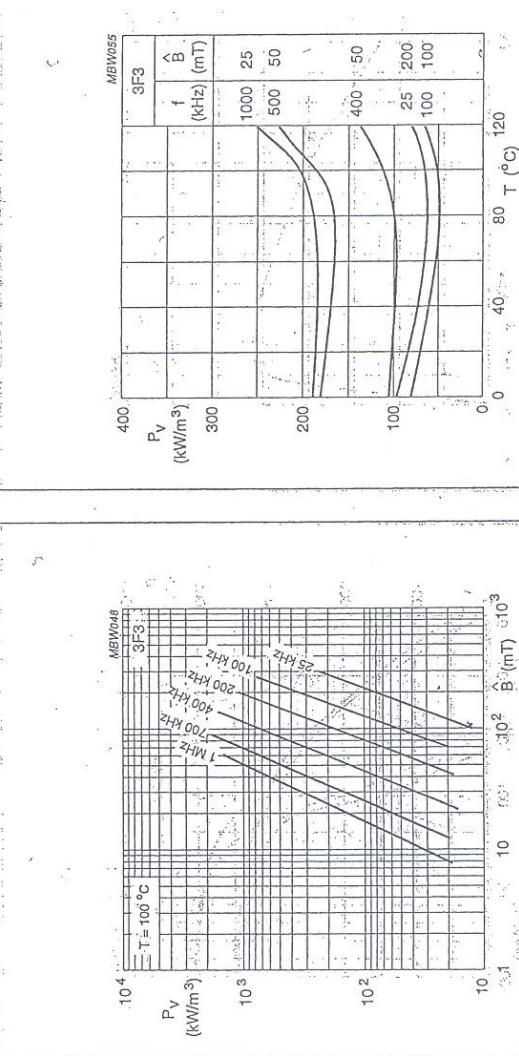
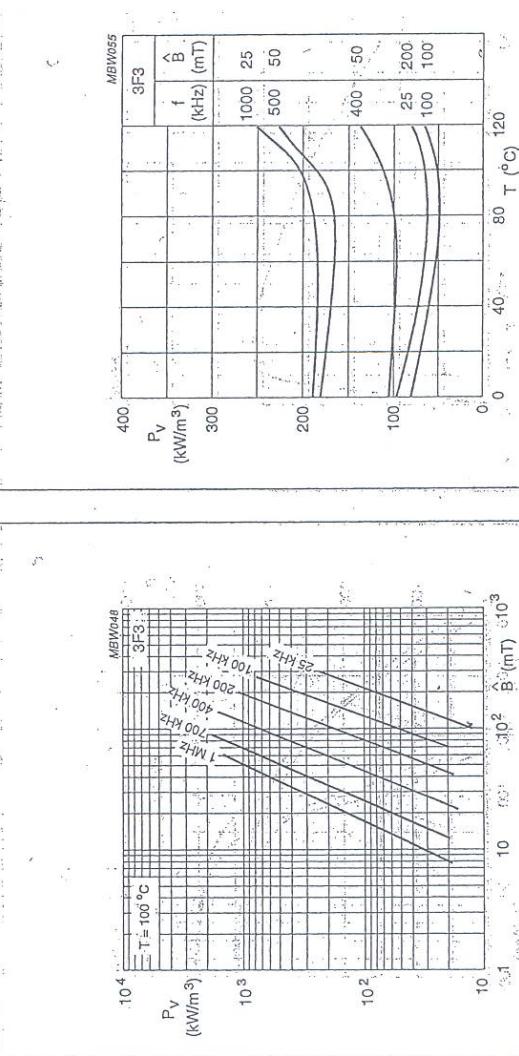
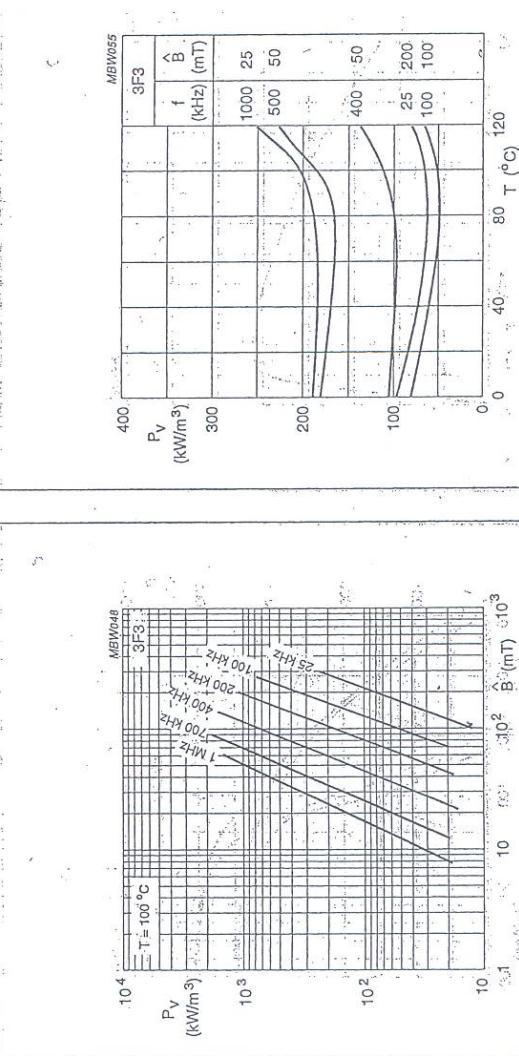
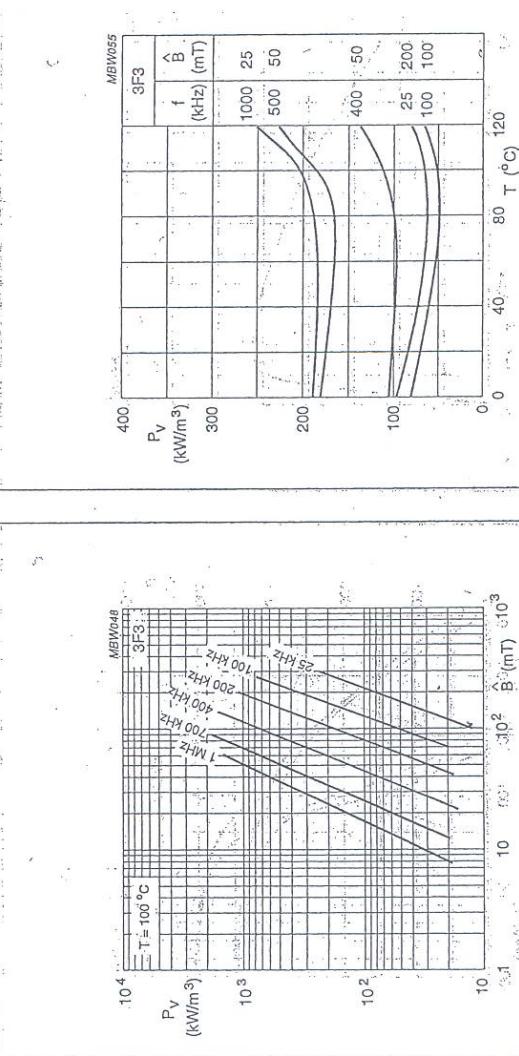
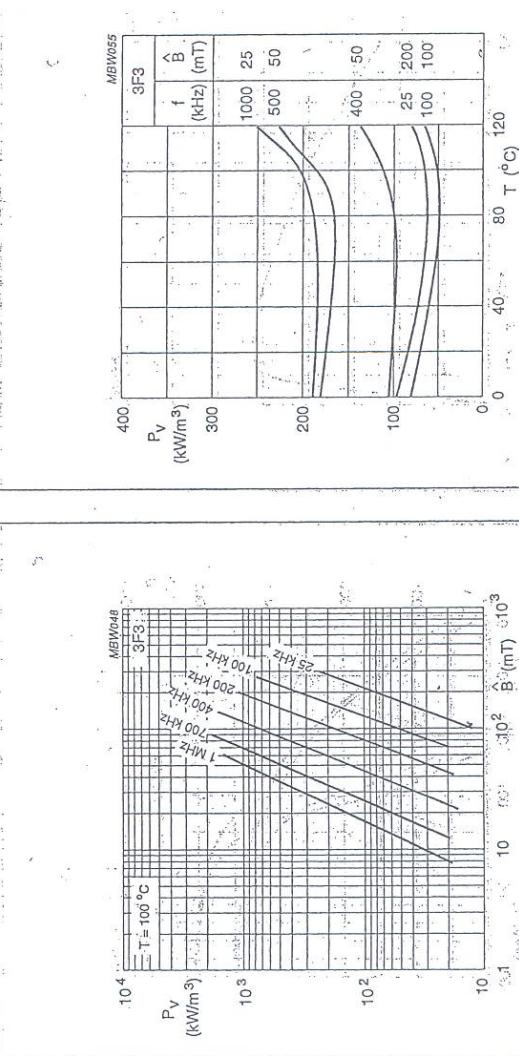
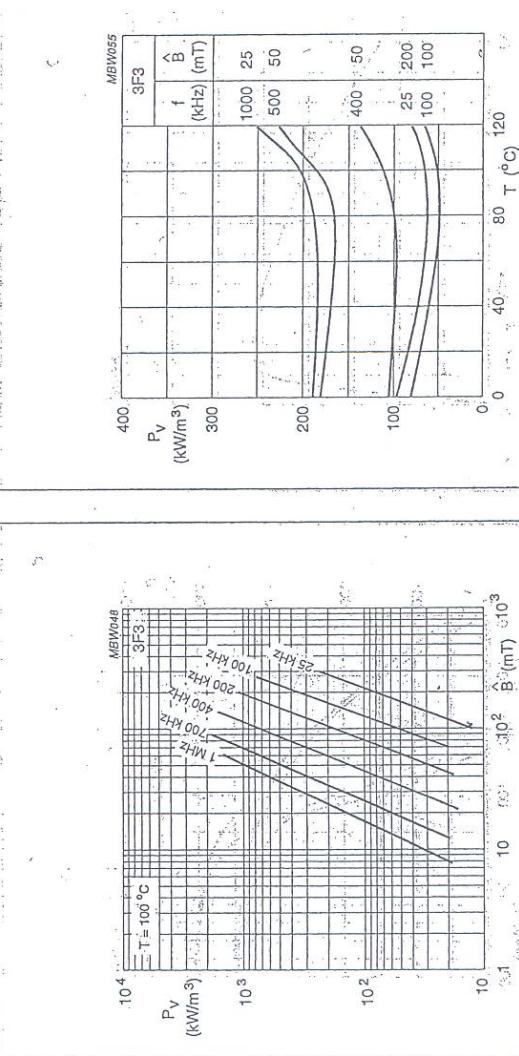
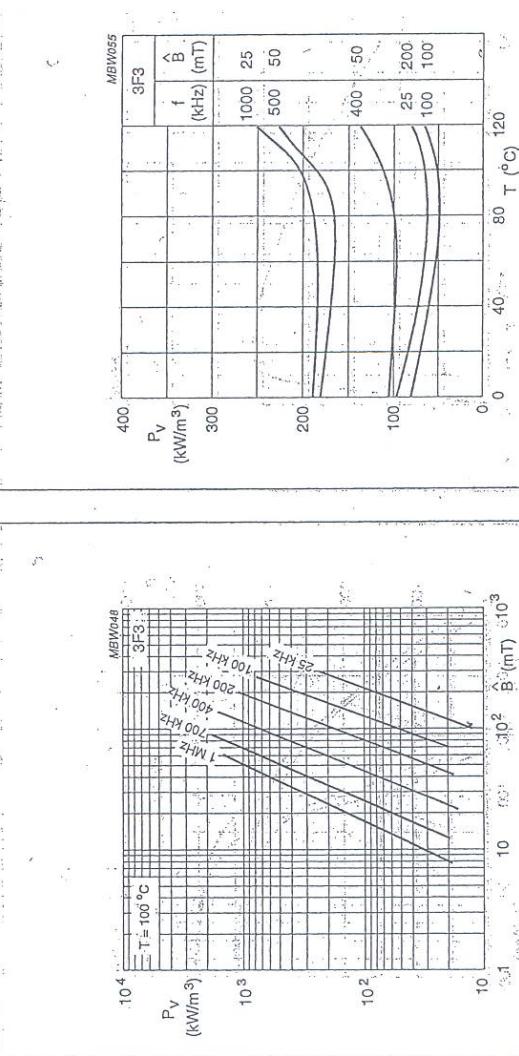
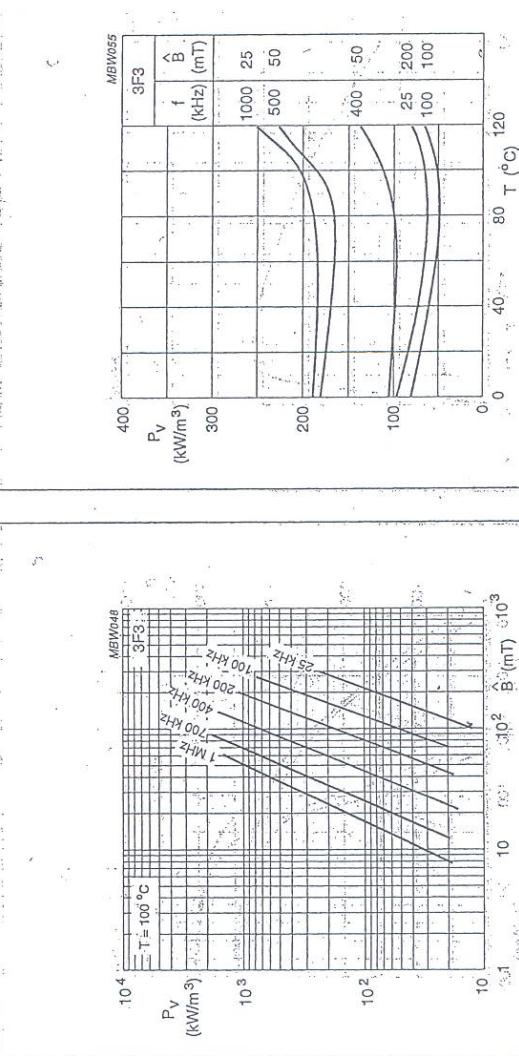
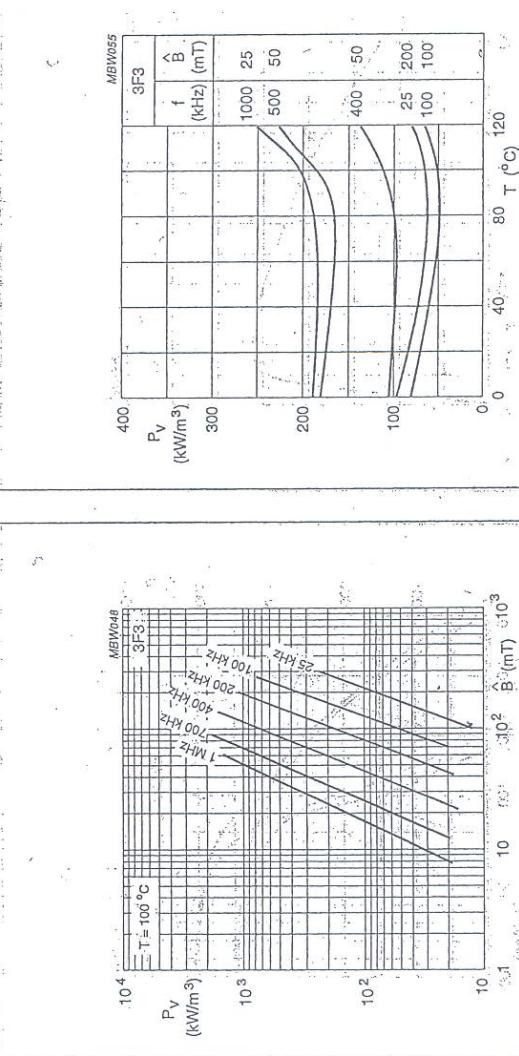
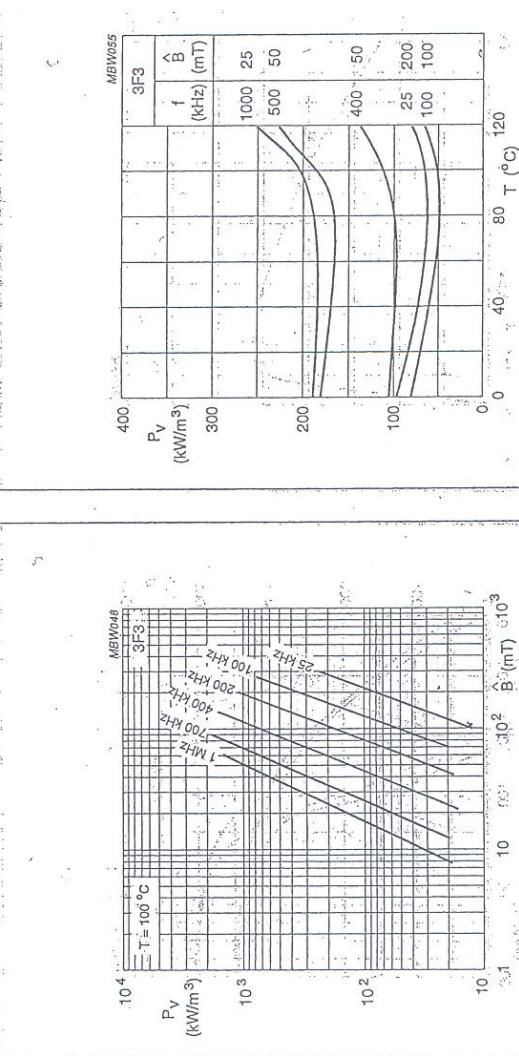
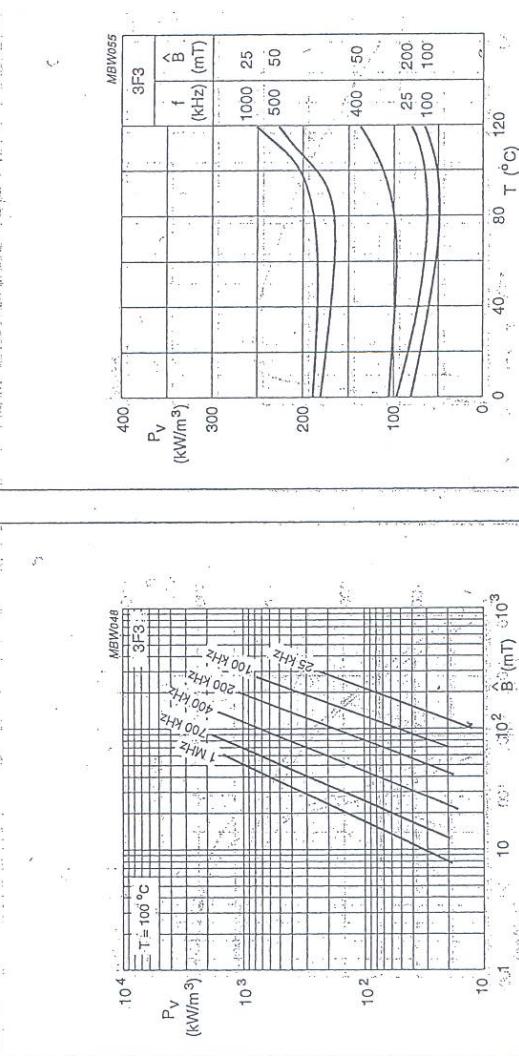
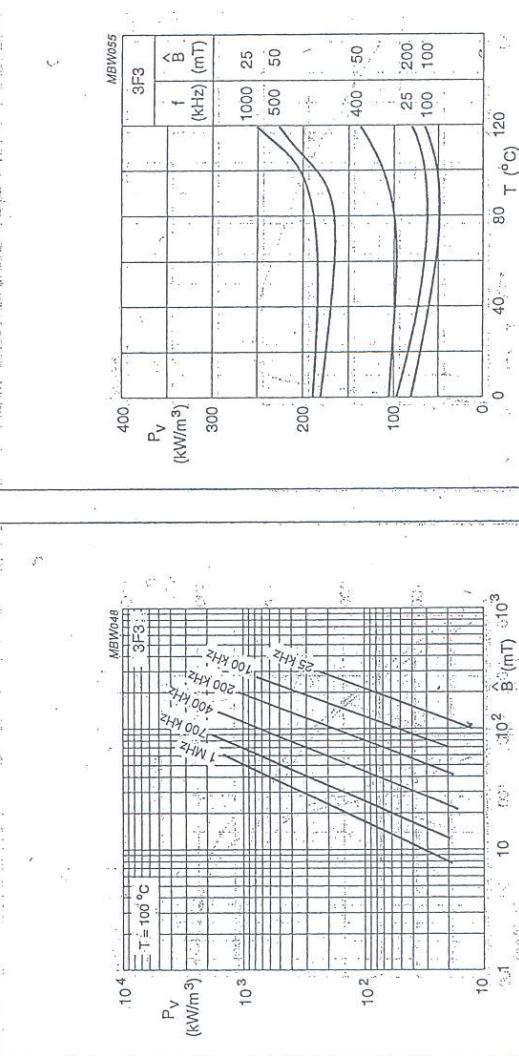
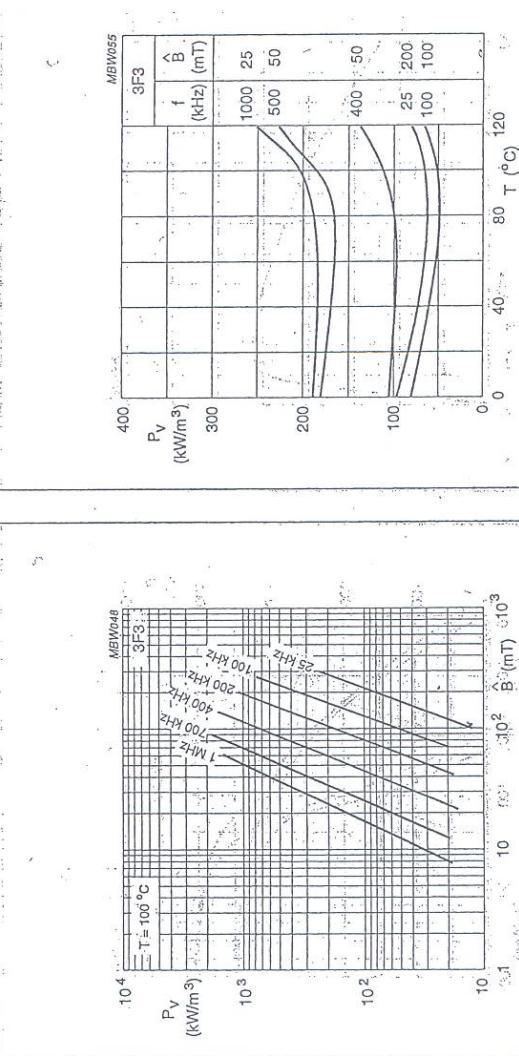
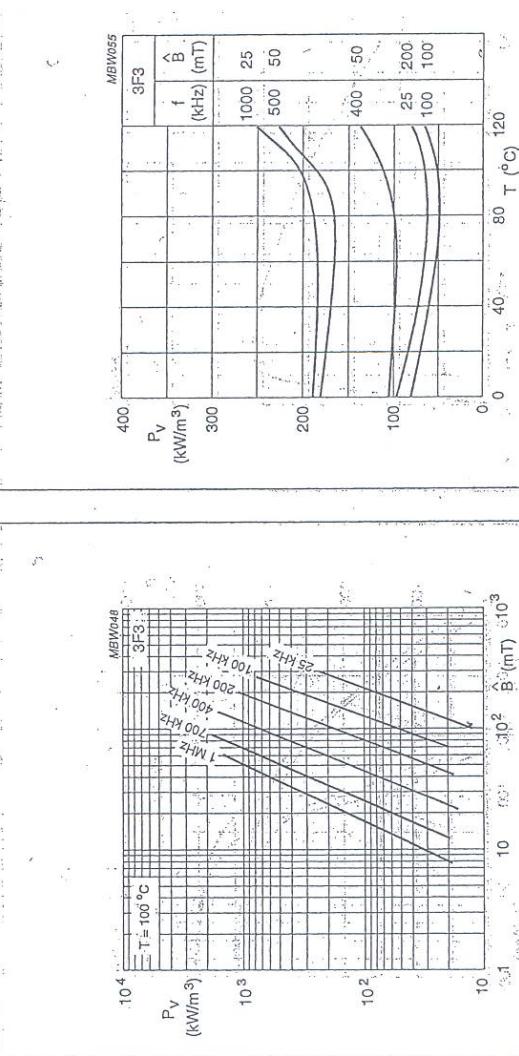
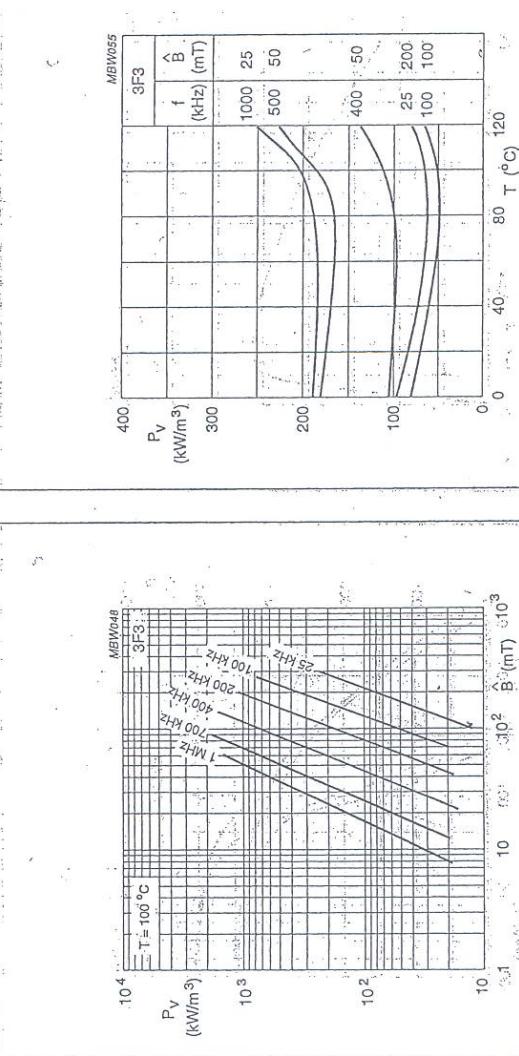
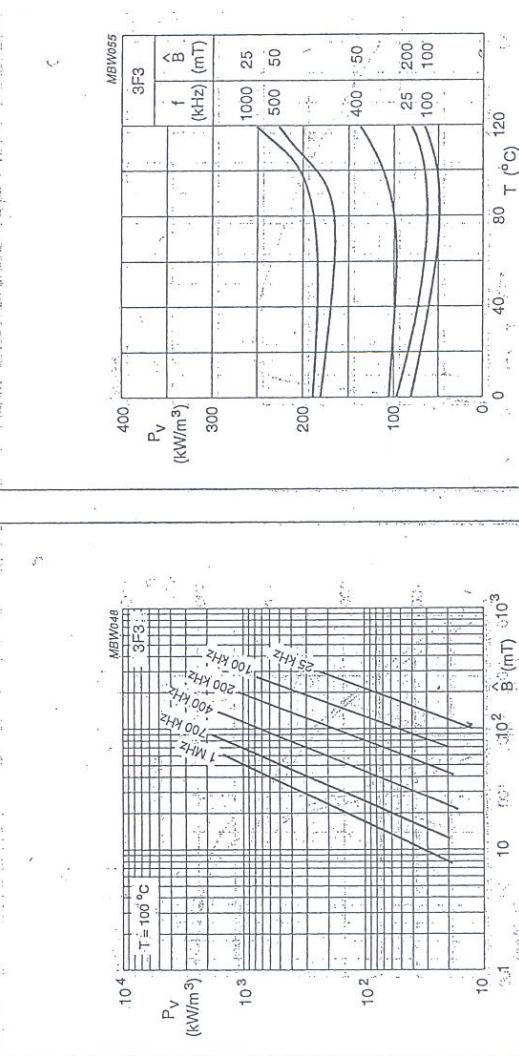
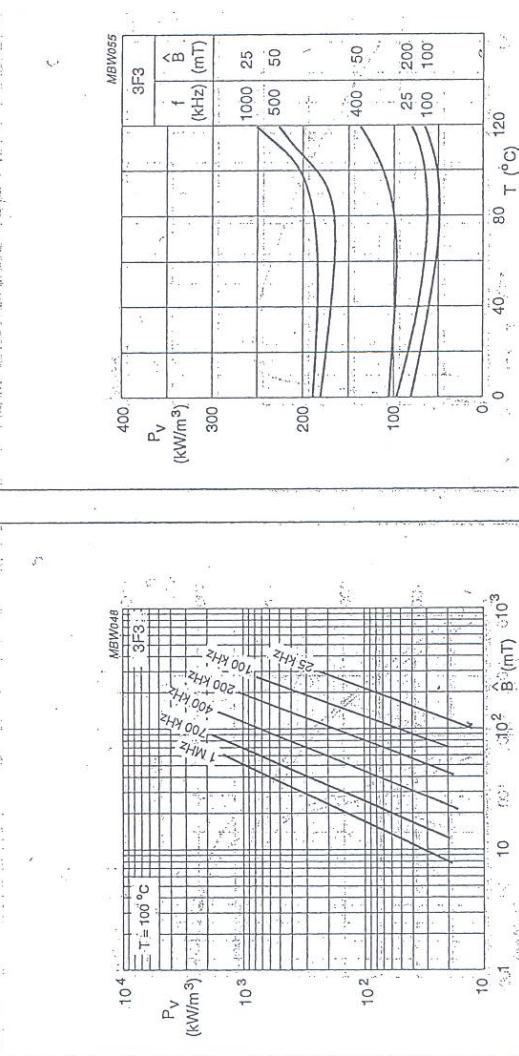
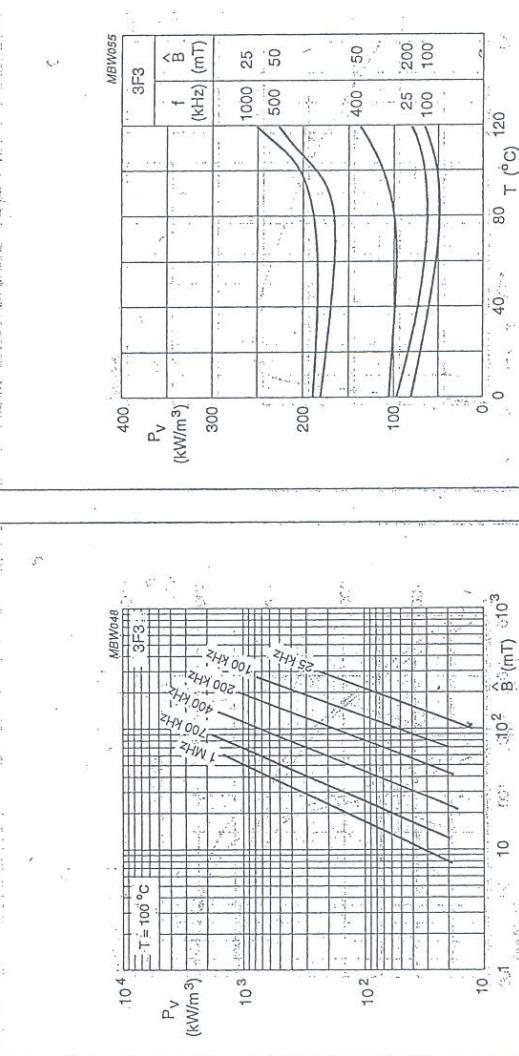
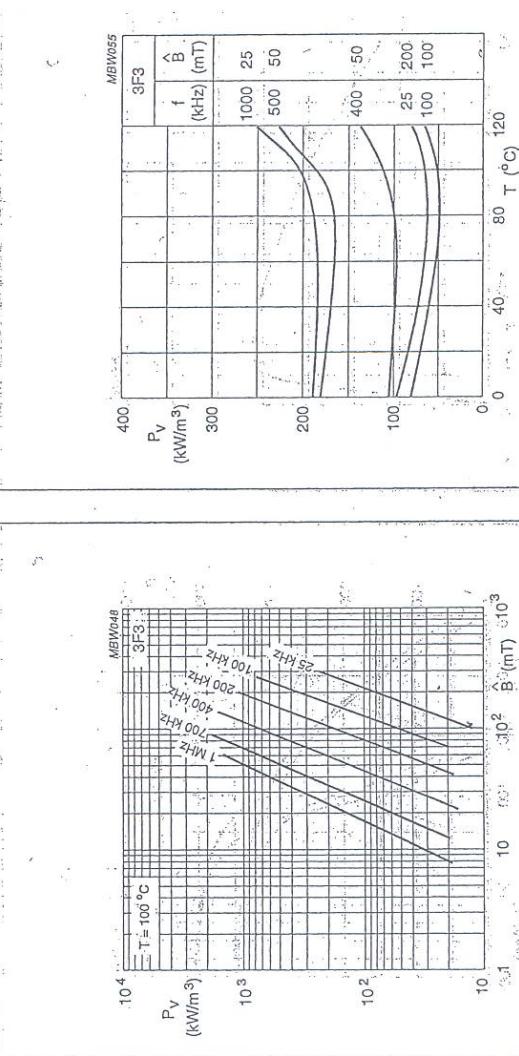
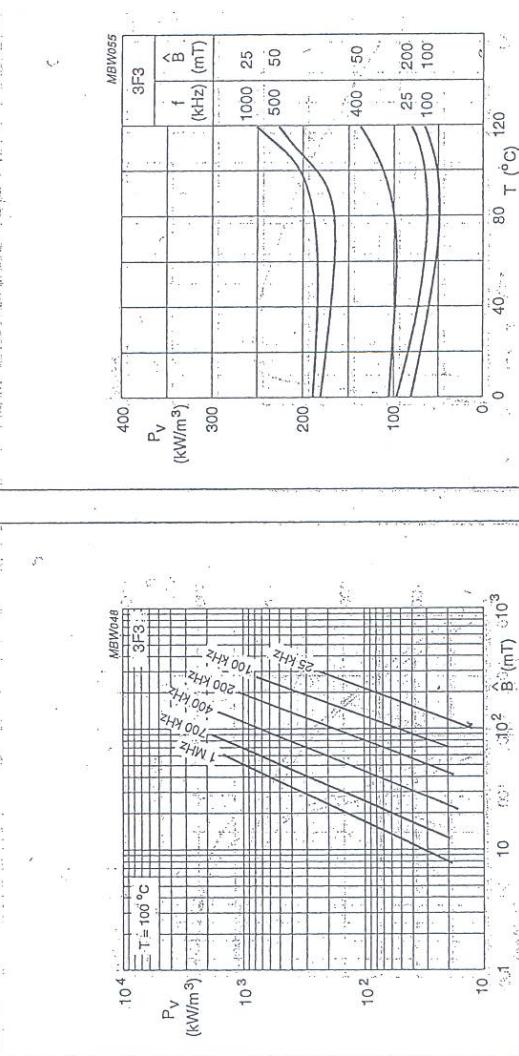
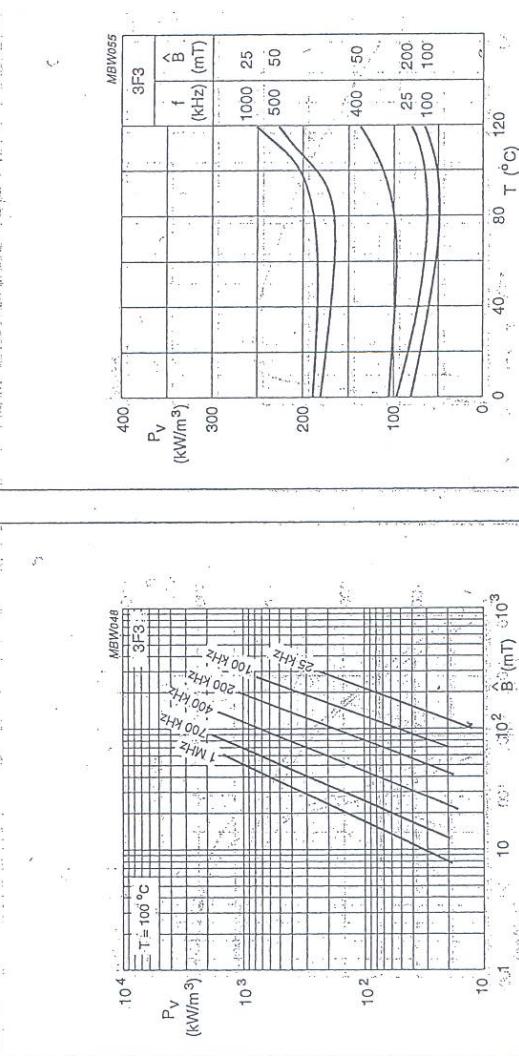
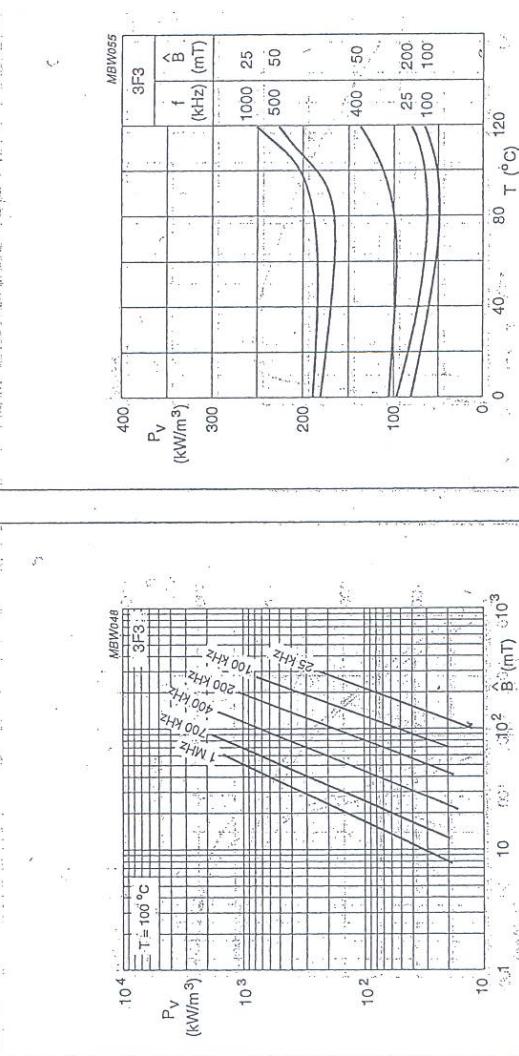
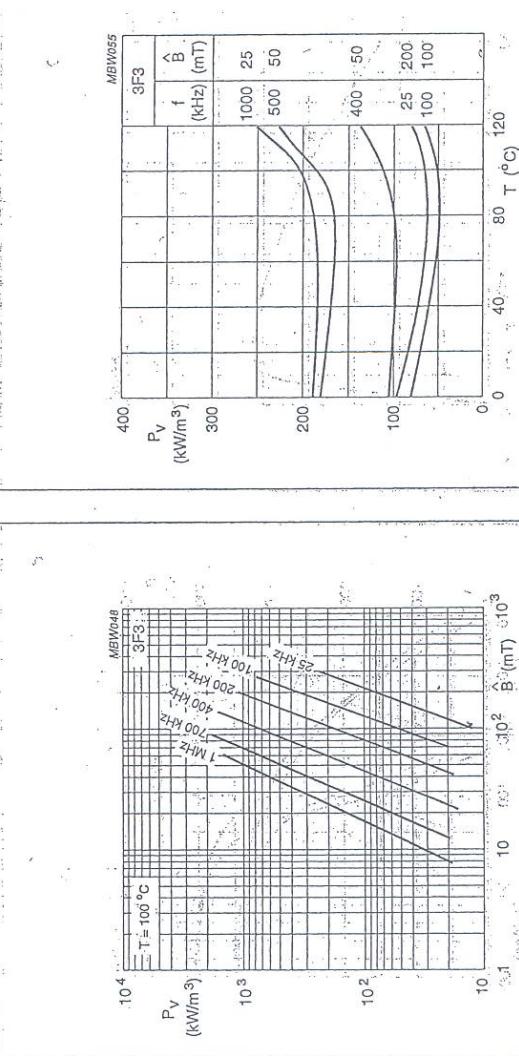
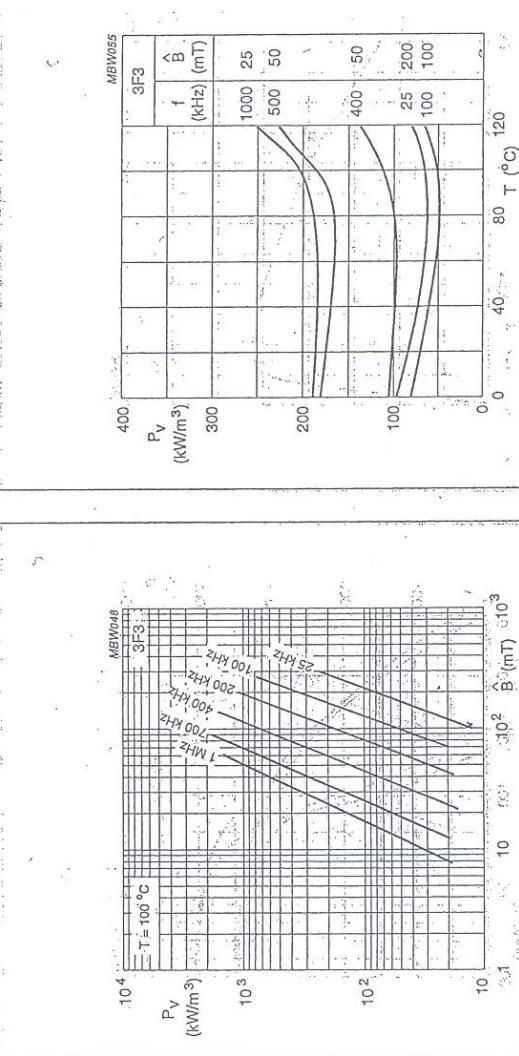
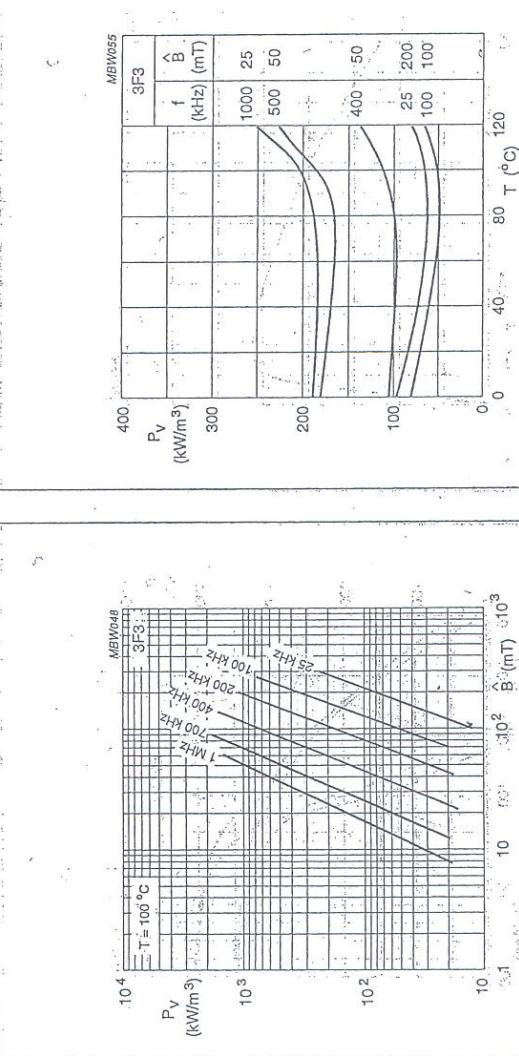
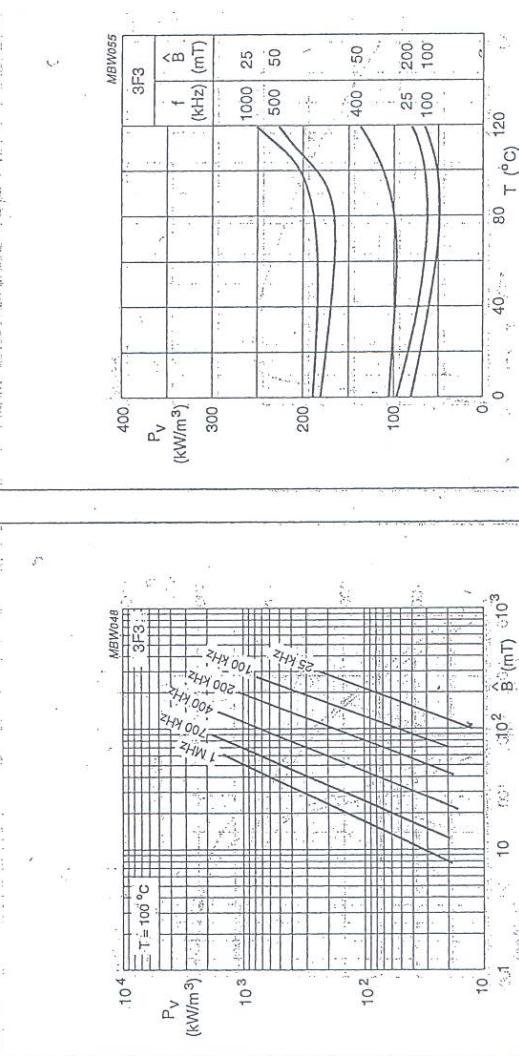
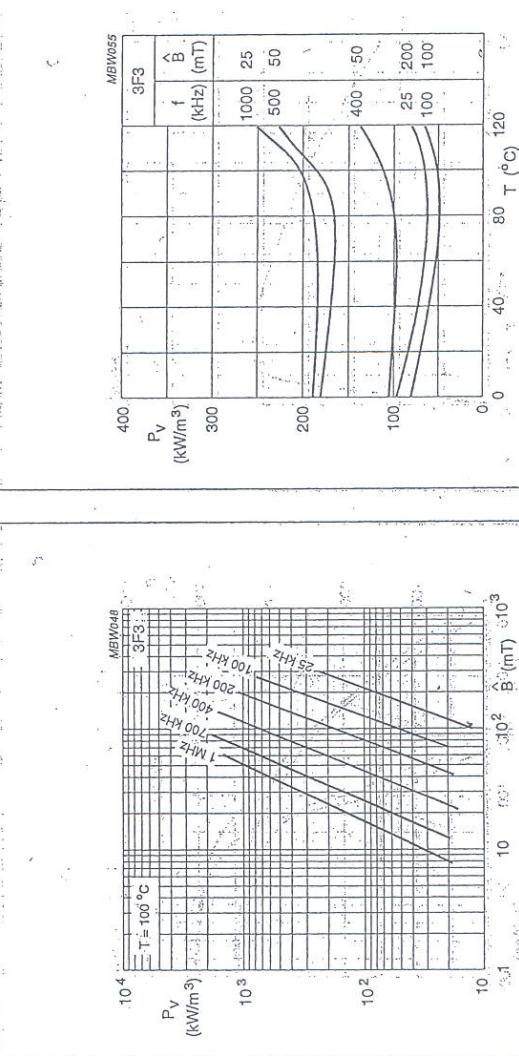
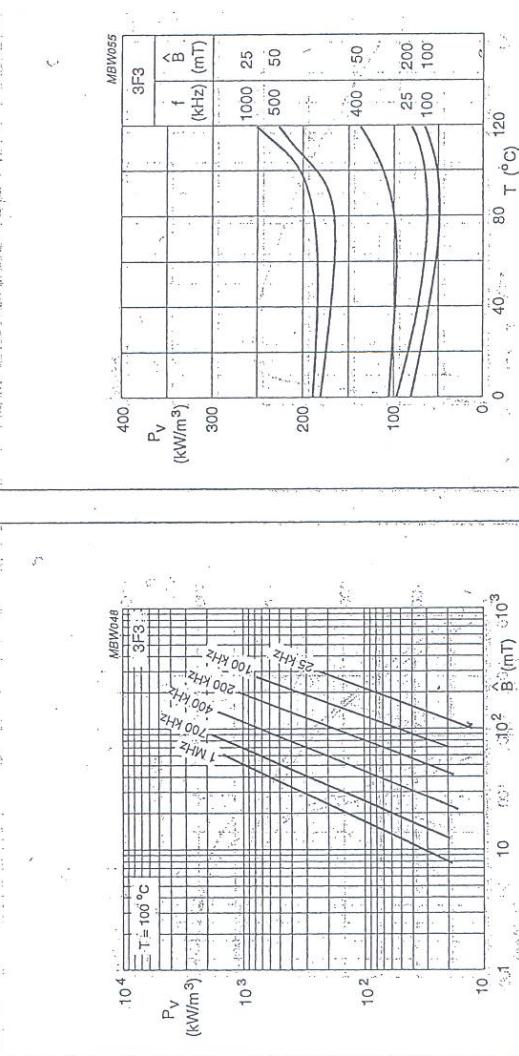
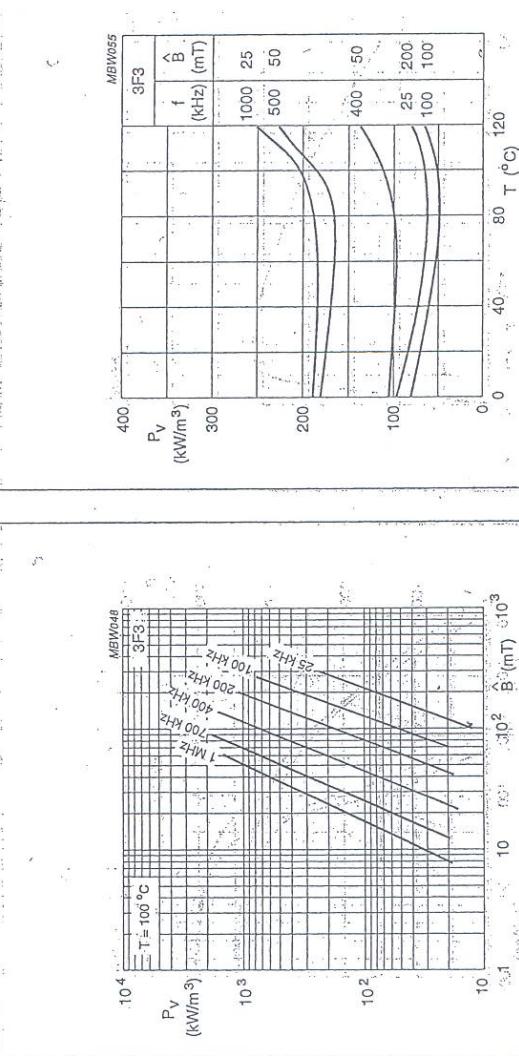
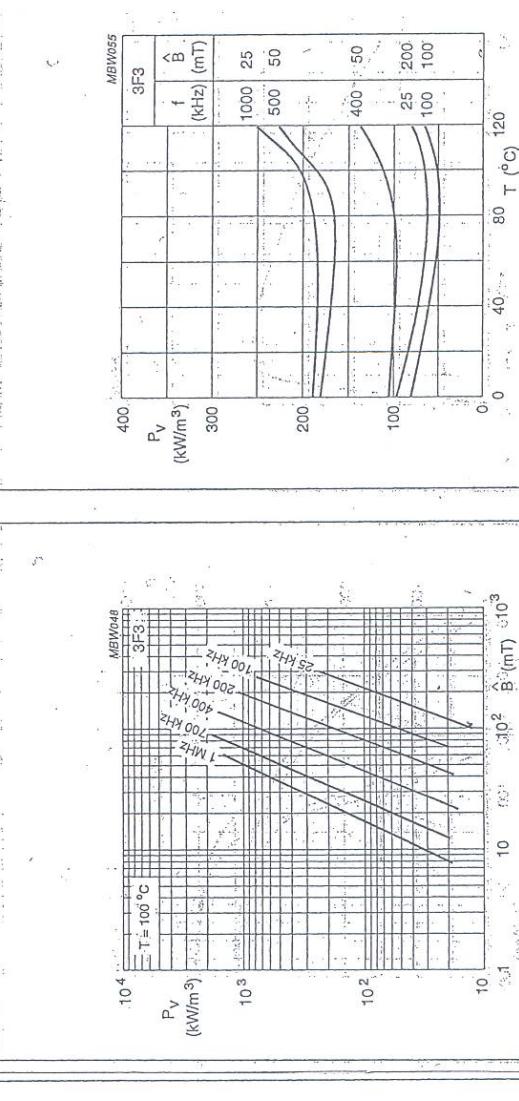
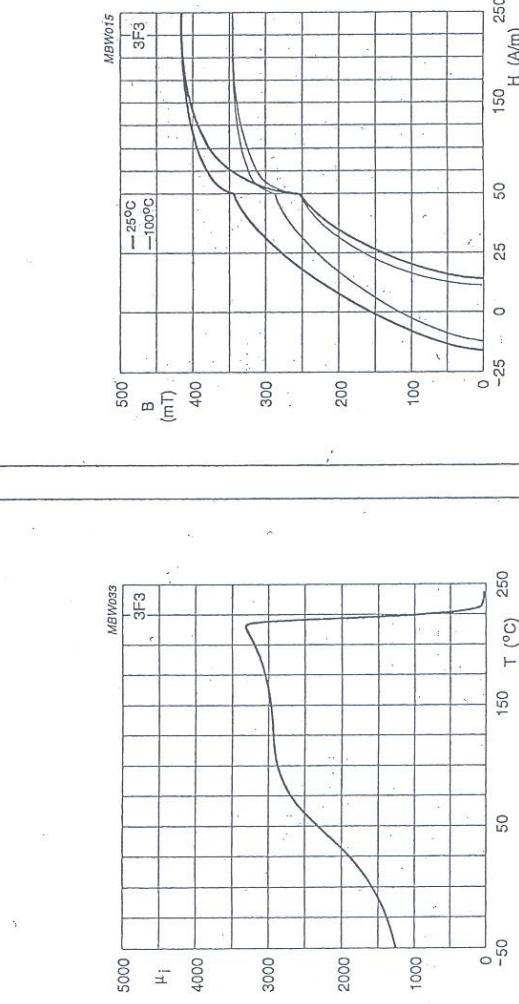


Fig.6 Specific power loss as a function of frequency/flux-density combinations as a function of temperature.



Conception des interfaces pour mesures adc
 Ampli op
 ad854x

fmax circuit = 7.957747e+004

Cadc min = 4.700000e-009

Capacité entrée convertisseur ad = 10e-9
 Fréquence de coupure = 8e3
 Affaiblissement critique
 ampli diff & filtre buffer
 conception 3ème ordre

R3 > 6.401684e+002
 R3normalise = 680

C2 = 2.205903e-009
 C2normalise = 1e-9

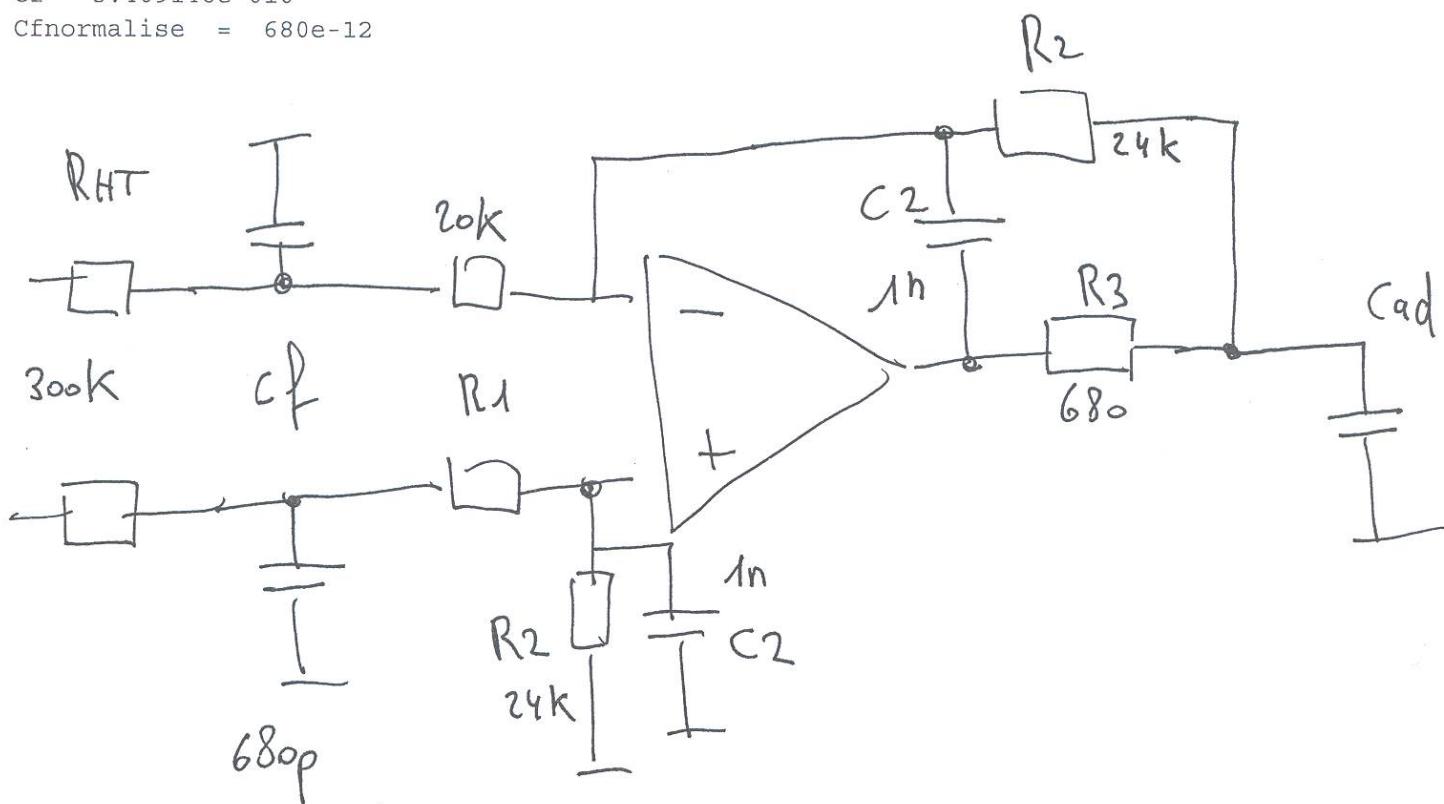
R2 = 2.410802e+004
 R2normalise = 24e3

Gain de mesure tension = 3/40
 Rht < 320000
 Rht = 300e3

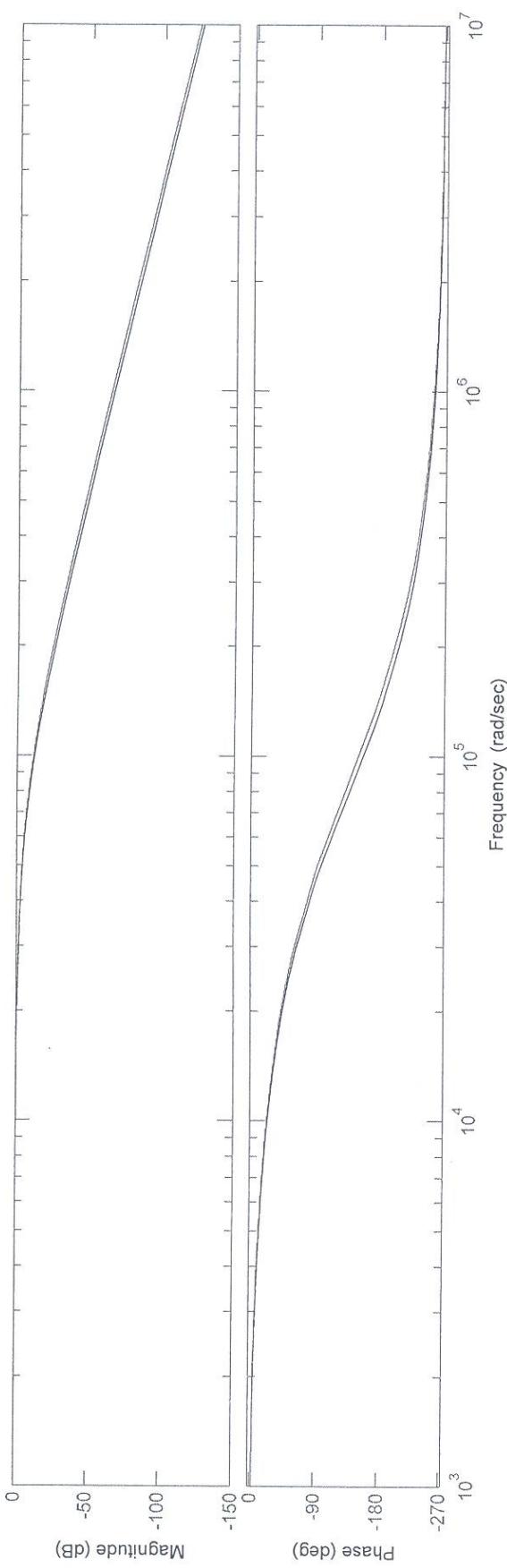
R1 = 20000
 R1normalise = 20e3

1/Gain normalisé = 1.333333e+001

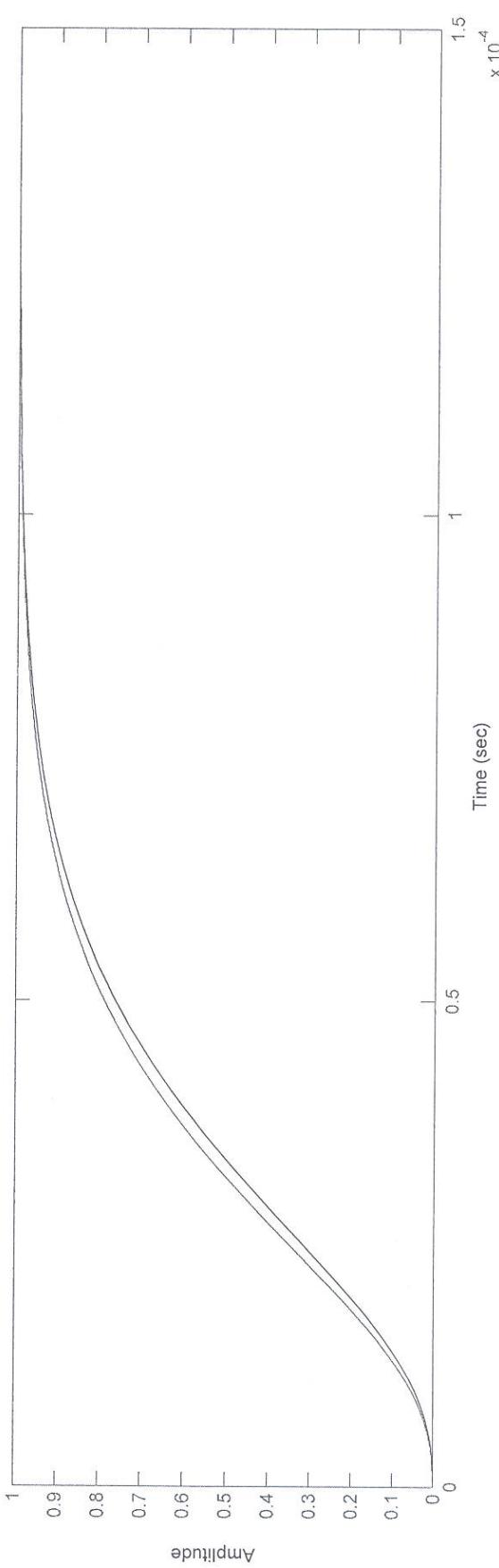
Cf = 5.409146e-010
 Cfnormalise = 680e-12

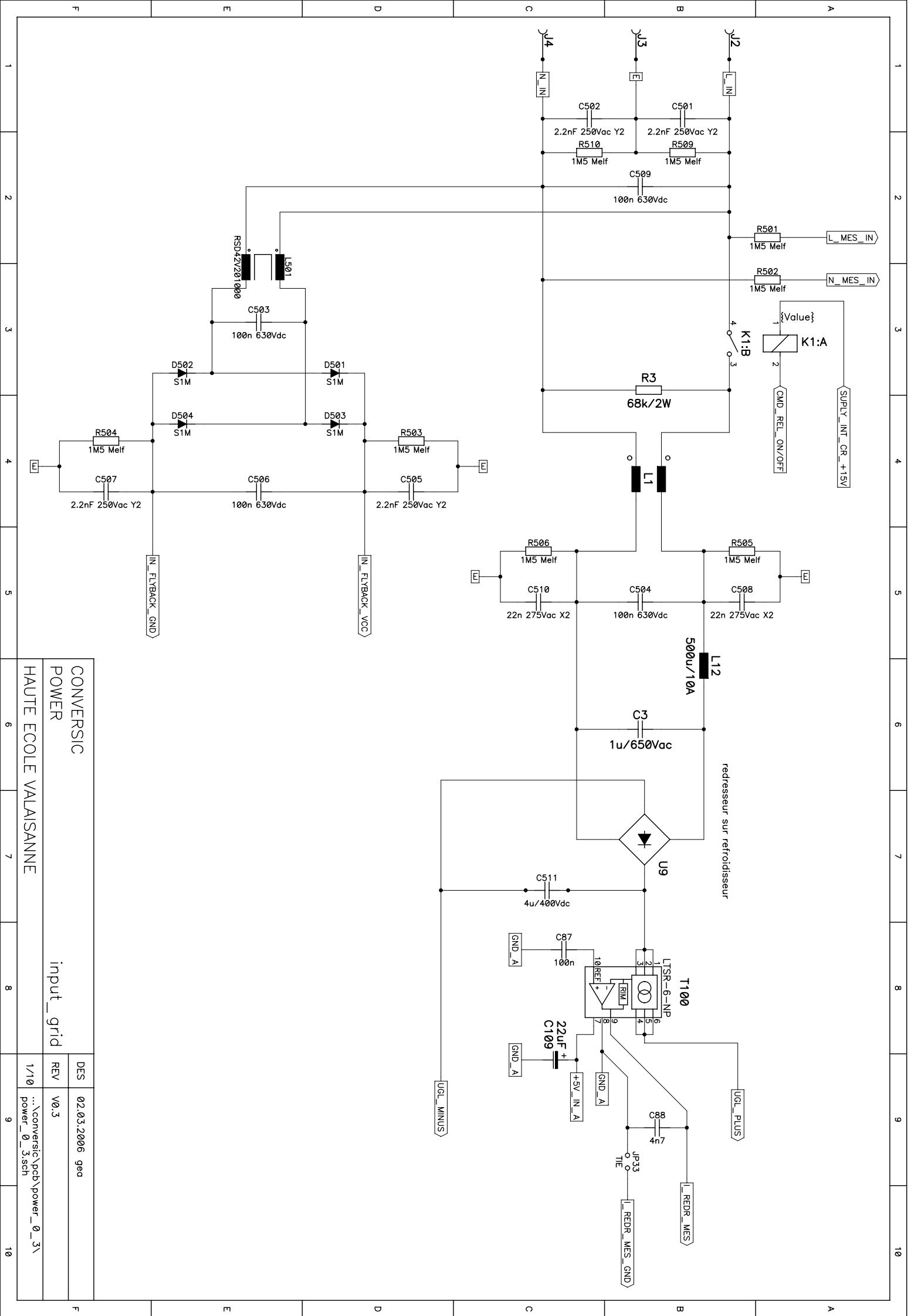


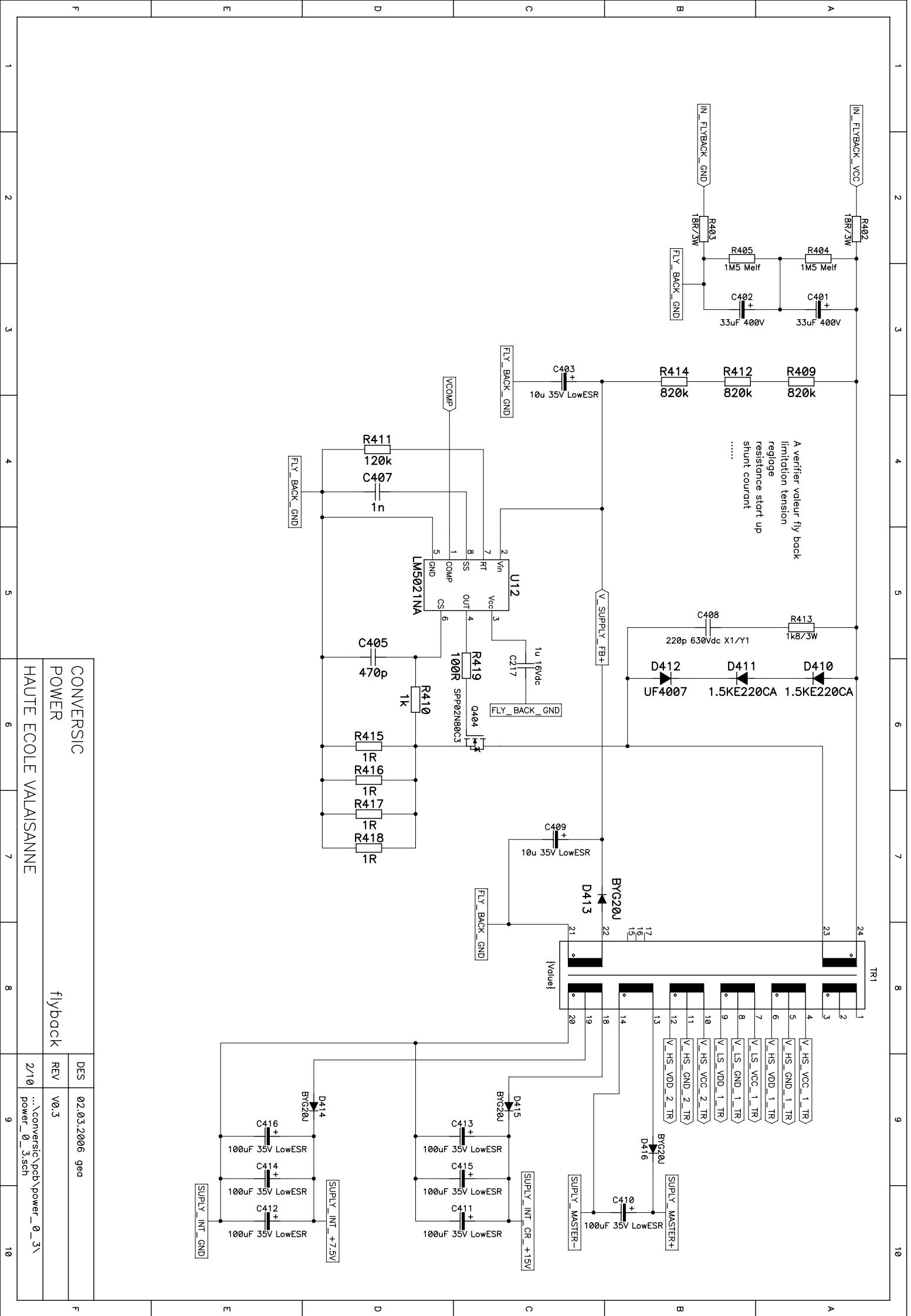
Bode Diagram

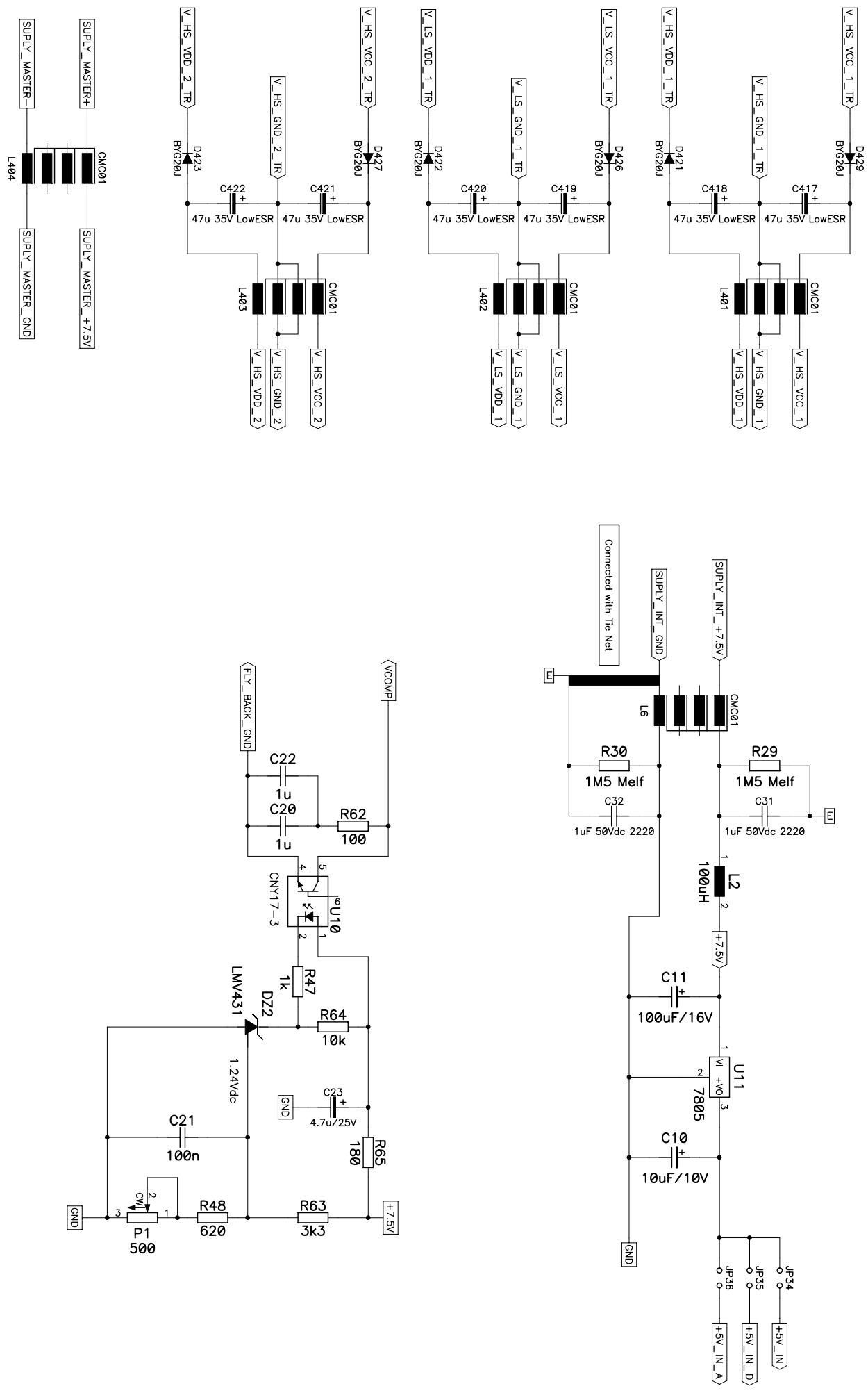


Step Response



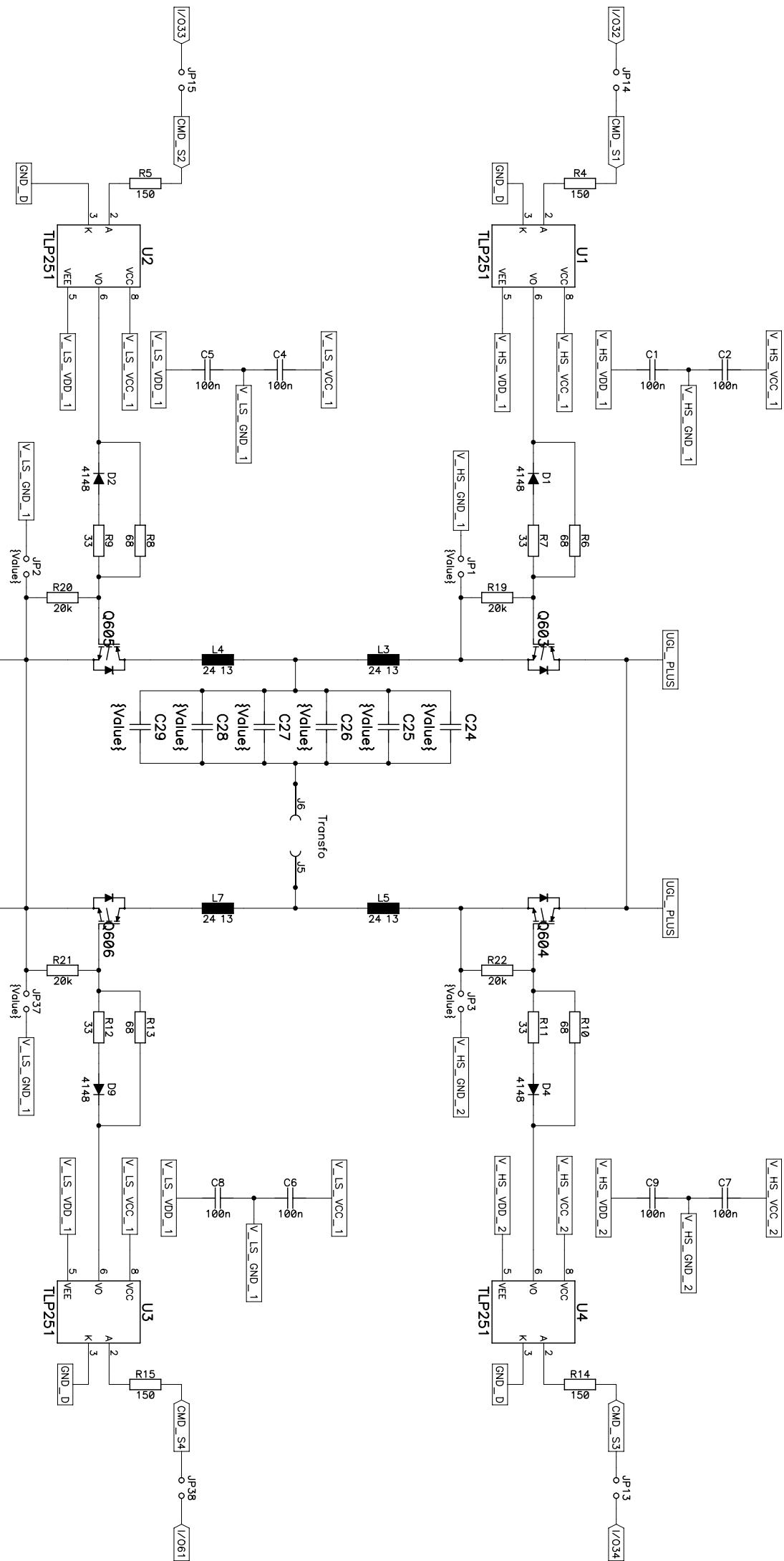






CONVERSIC	DES	02.03.2006 gea
POWER	REV	V0.3
HAUTE ECOLE VALAISANNE		3/10 ... \conversic\pb\power_0_3\ power_0_3.scn

1 2 3 4 5 6 7 8 9 10



1 2 3 4 5

6 7 8

9 10

E

A 1 B 2 C 3 D 4 E 5 F 6 G 7 H 8 I 9 J 10

CONVERSIC	DES	02.03.2006	geo
POWER	REV	V0.3	libre
HAUTE ECOLE VALAISANNE		5/10	..\conversic\pcd\power_0_3\power_0_3.sch
		9	
		10	

F	E	D	C	B	A
1	2	3	4	5	6
5	4	3	2	1	
6	7	8	9	10	

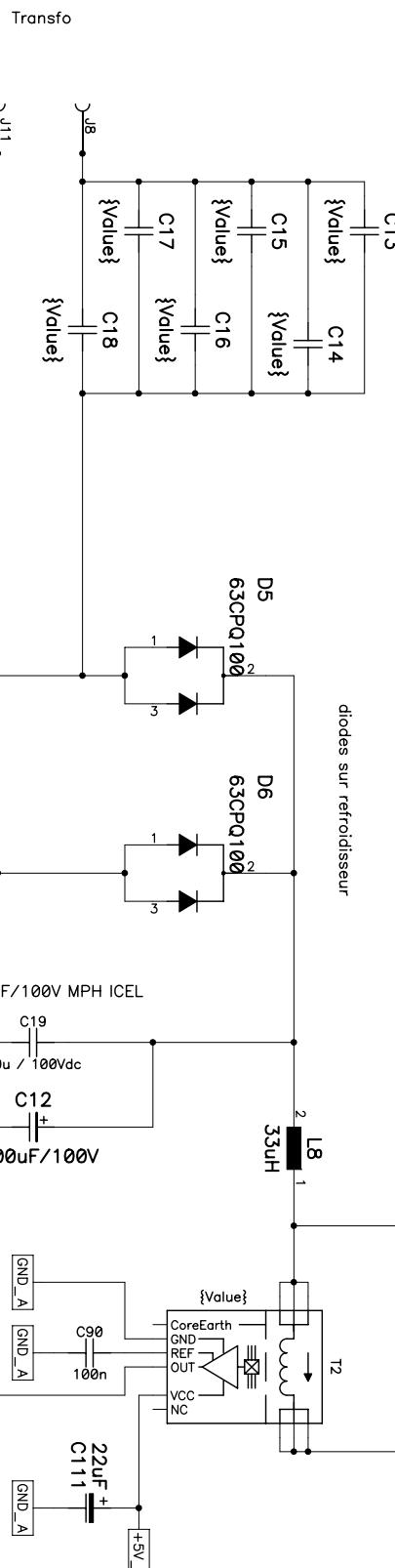
1 2 3 4 5 6 7 8 9 10

100Vdc / 50->100A

Capteur HALL TP

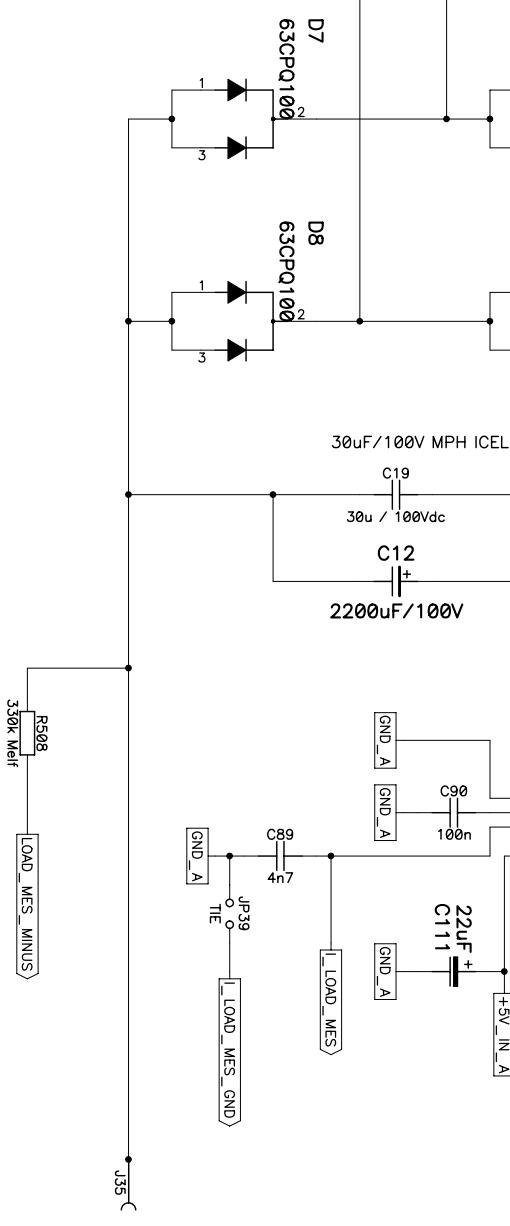
R507
30k Melf
LOAD_MES_PLUS

J12



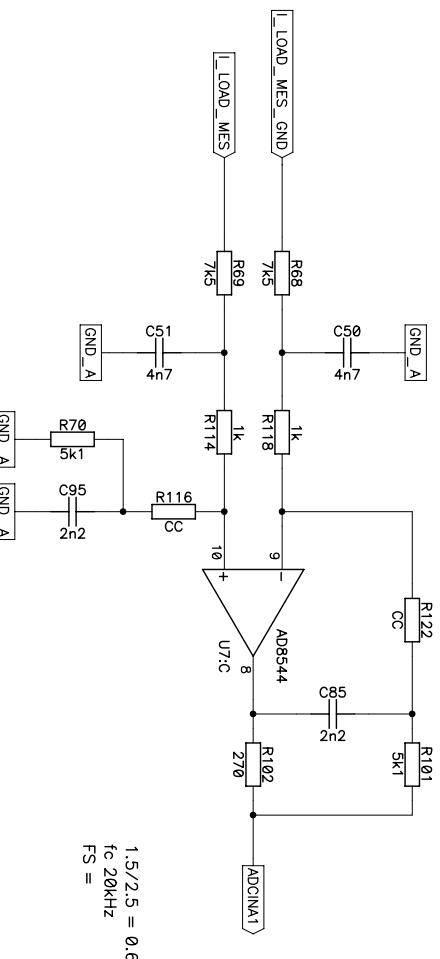
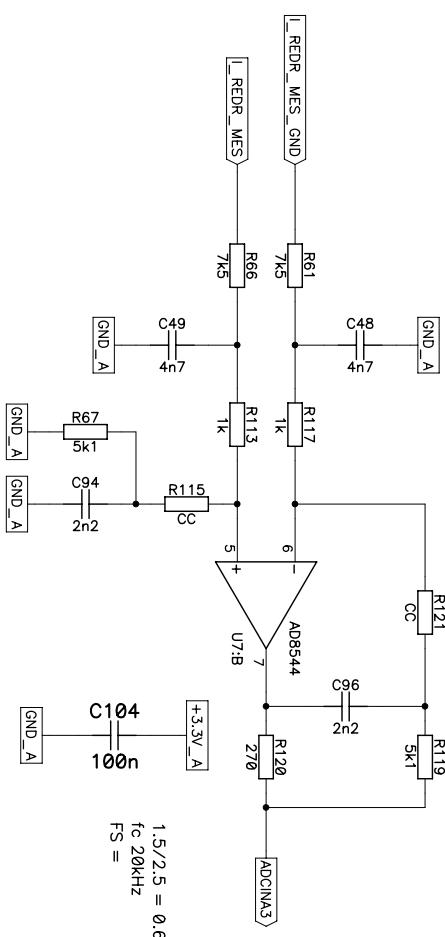
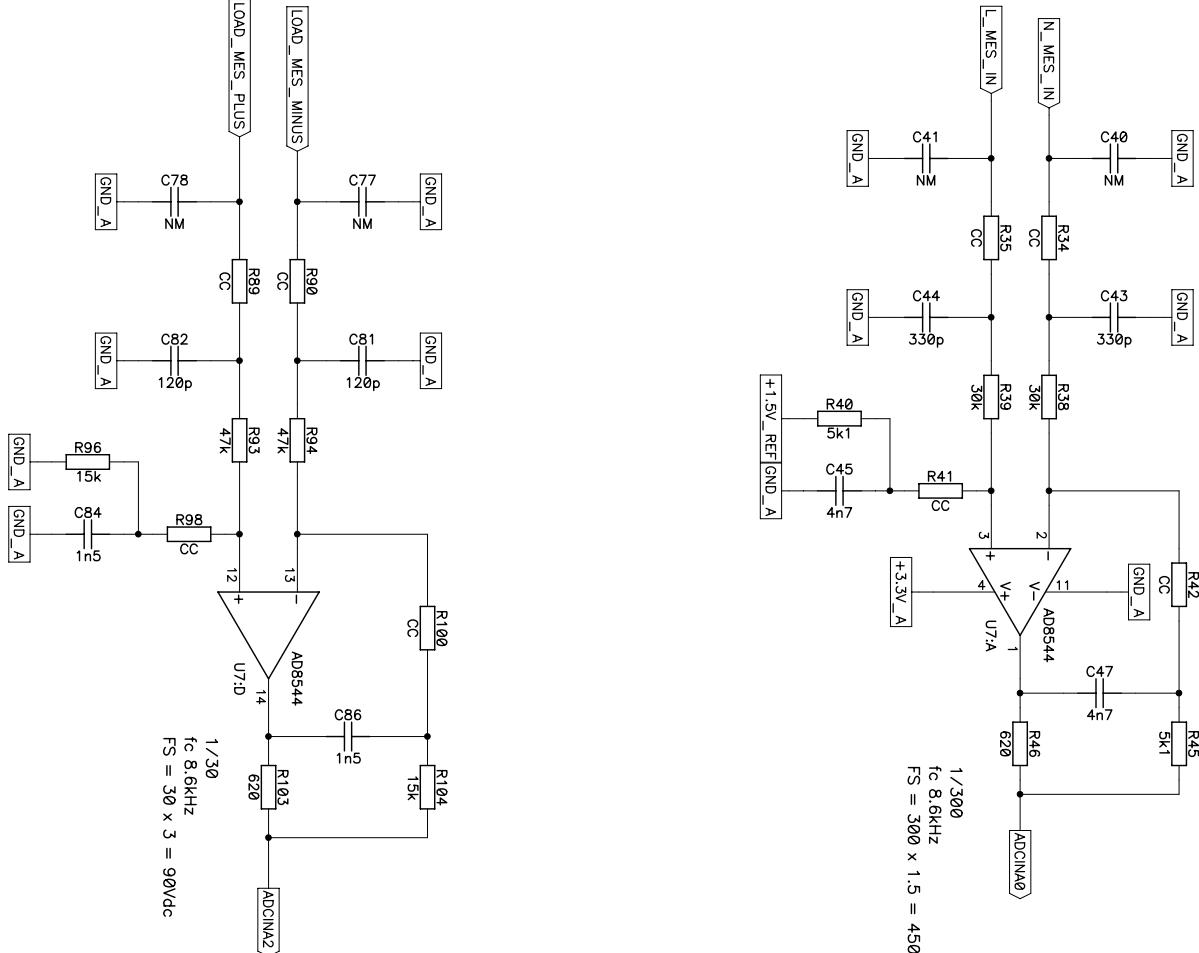
diodes sur refroidisseur

Transfo

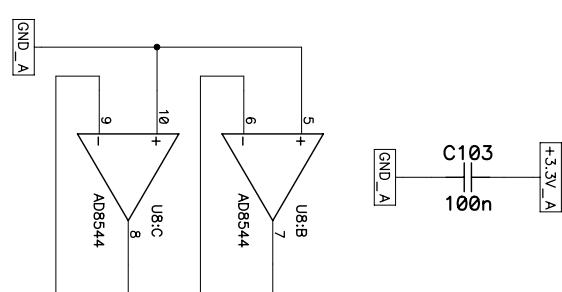
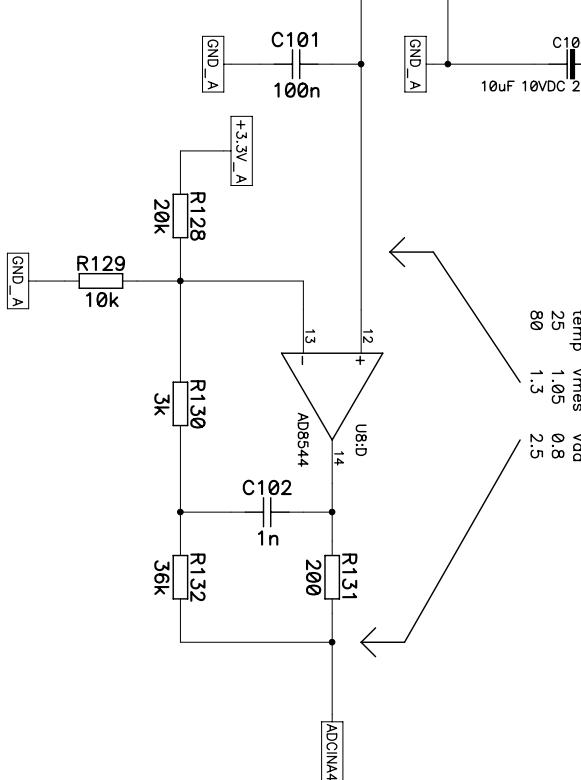
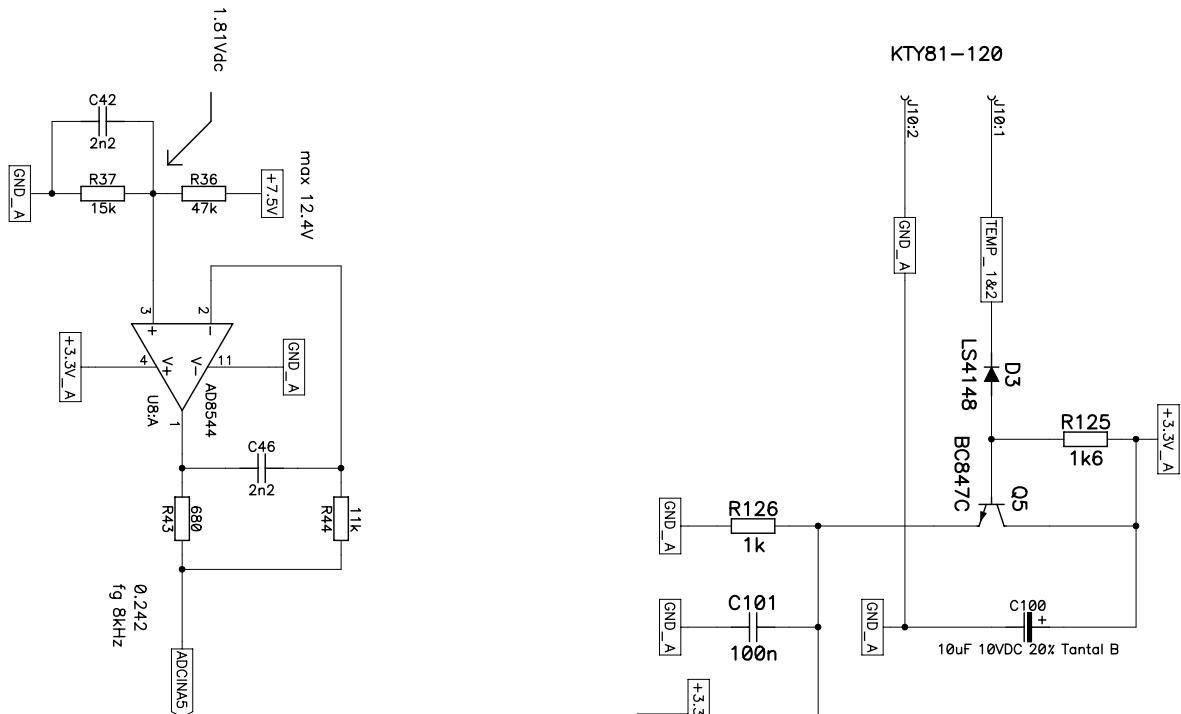


CONVERASIC	DES	02.03.2006 gca
POWER	REV	V0.3
HAUTE ECOLE VALAISANNE		..\converasic\pcd\power_0_3\
		6/10 power_0_3.sch
1	2	3
4	5	6
7	8	9
10		10

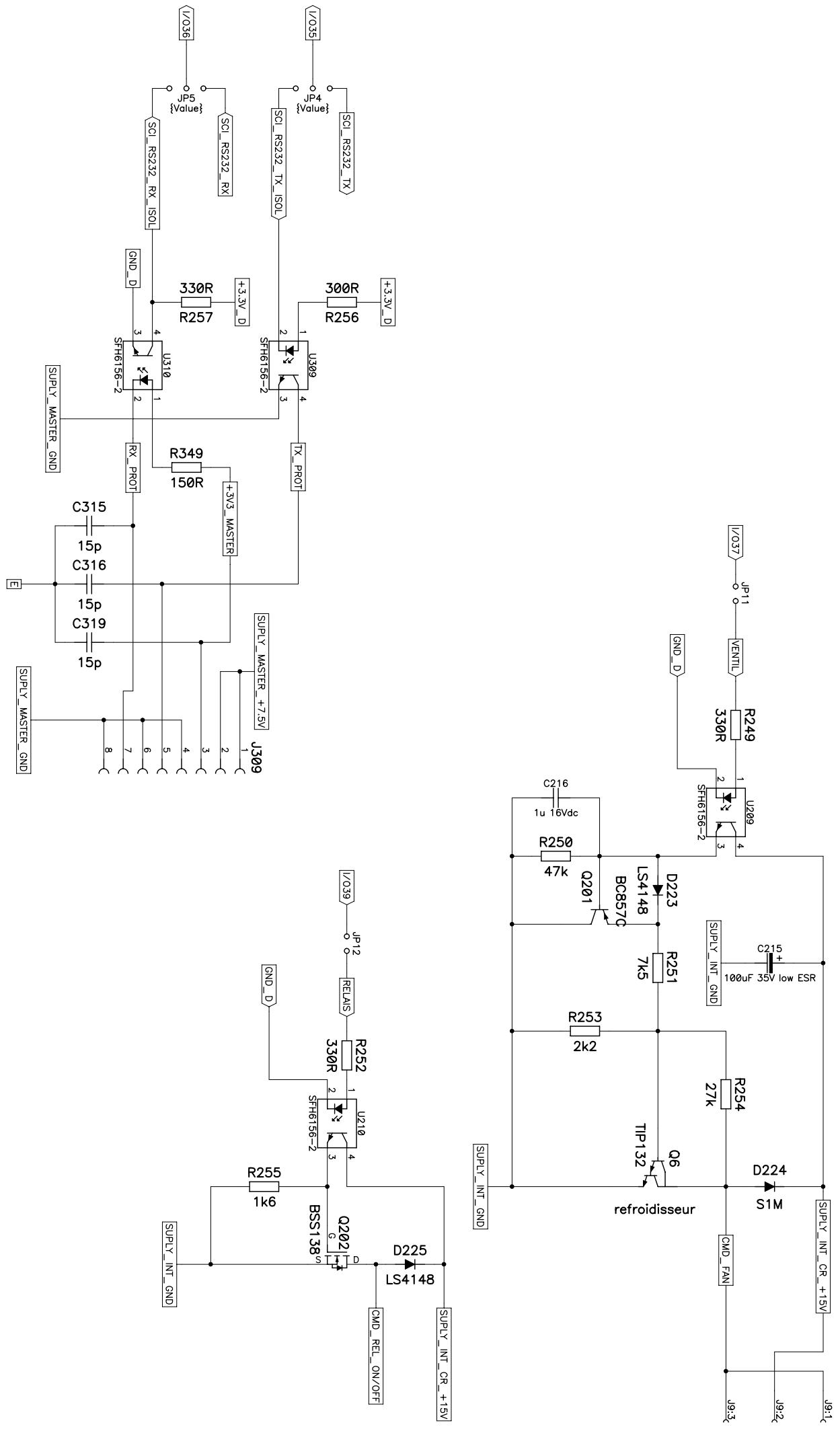
1 2 3 4 5 6 7 8 9 10



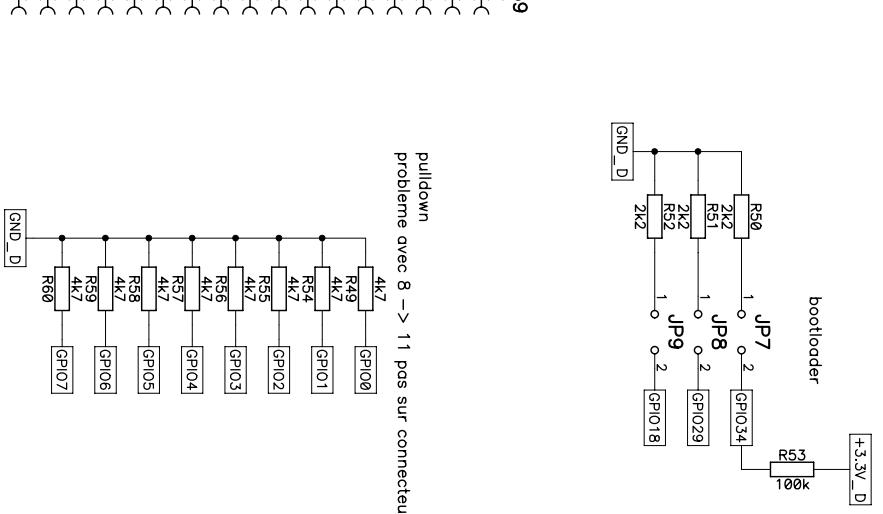
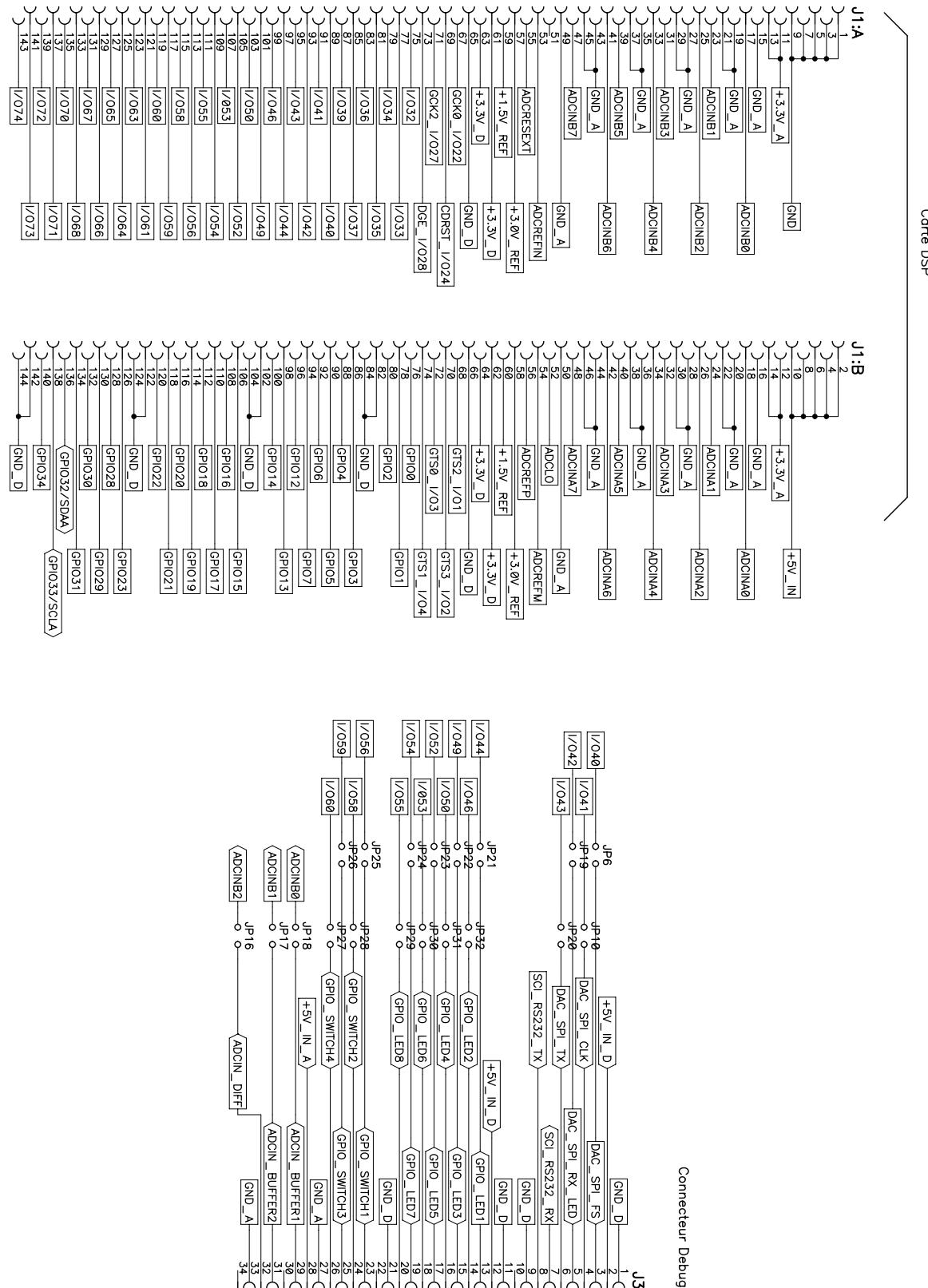
CONVERSI		DES	02.03.2006 gca
POWER		REV	V0.3
measures 1		..\convertic\pcd\power_0_3.sch	
7/10	power_0_3.sch		
1		2	
3		4	
5		6	
7		8	
8		9	
9		10	



CONVERSI	DES	02.03.2006 gca
POWER	REV	V0.3
measures 2		..\conversic\pcb\power_0_3.sch
HAUTE ECOLE VALAISANNE		8/10 power_0_3.sch
1	2	3
4	5	6
7	8	9
10		



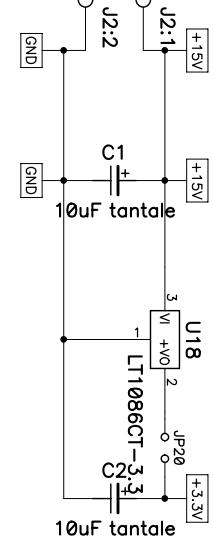
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HAUTE ECOLE VALAISANNE		...\\conversic\\pcb\\power_0_3\\power_0_3.sch	9/10



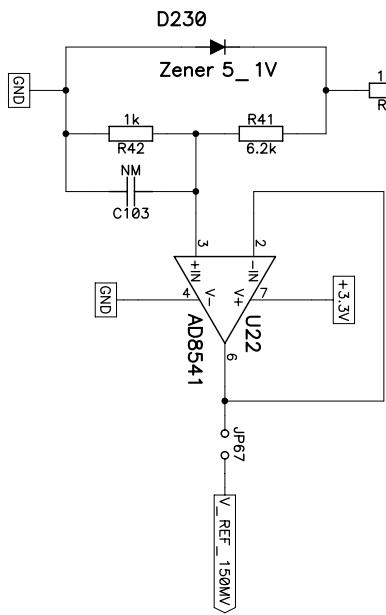
CONVERSIC	DES	02.03.2006 gca
POWER	REV	v0.3
HAUTE ECOLE VALAISANNE	module	144
	10/10	... \conversic\pb\power_0_3\power_0_3.scn

1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10

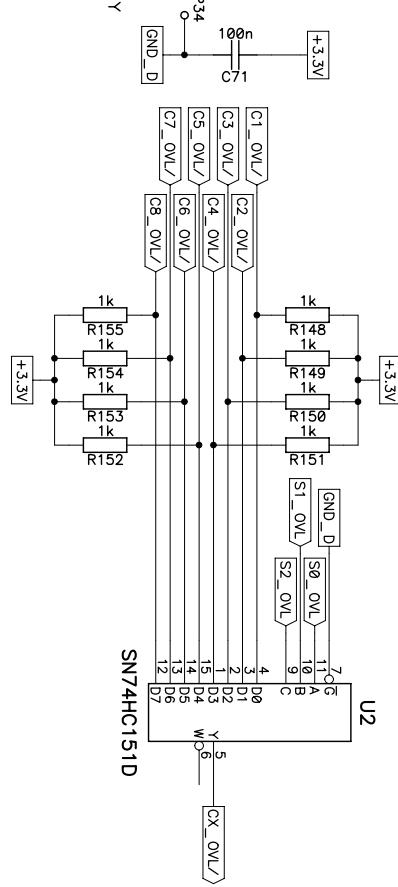
Alimentation Principale
prise au primaire



Reference 150mV/proche des 8 canaux

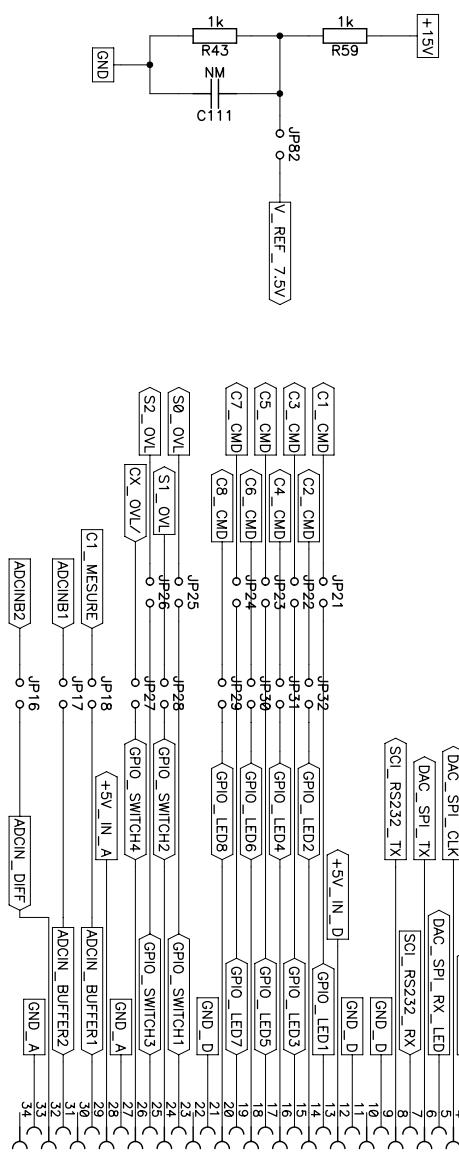


Mux les 8 overloads en 4 signaux



Connecteur Primaire/DSP

Reference 7.5V/ proche du det_courant



Mesure de Uout effectuée au primaire

J1:1 └── UOUT_PLUS
J1:2 └── UOUT_MINUS

DIMMER ACL
POWER & CONTROL
HAUTE ECOLE VALAISANNE

DES 19.10.2007 Jerome Gerber
REV V1.0
D:\ACL\PC-CAD
Secondaire_acl.sch

1 | 2 | 3 | 4 | 5

6

7

8

9

10

E

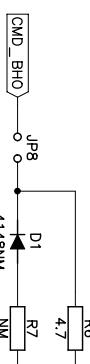
F

Pont redresseur actif

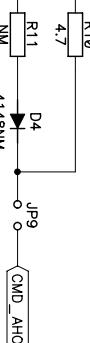
UOUT_PLUS

UOUT_MINUS

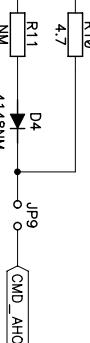
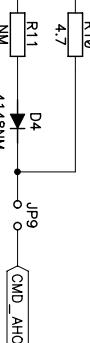
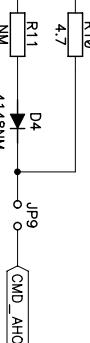
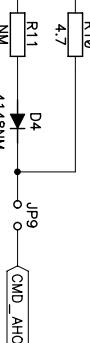
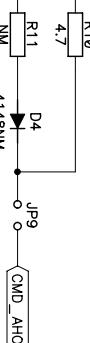
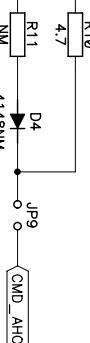
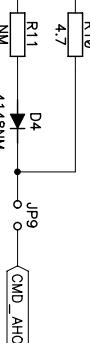
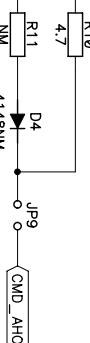
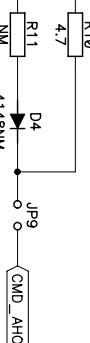
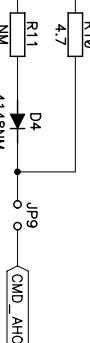
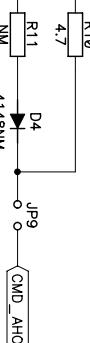
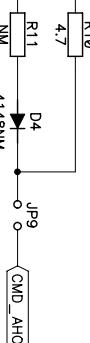
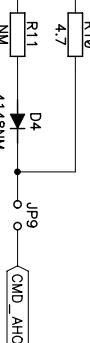
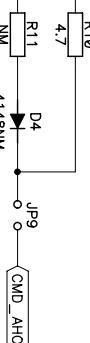
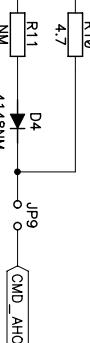
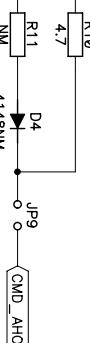
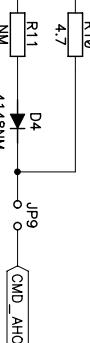
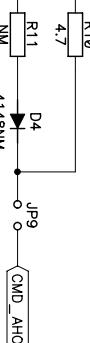
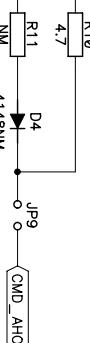
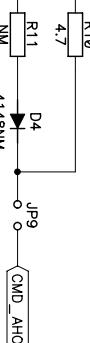
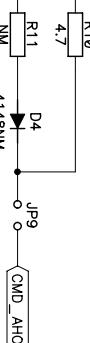
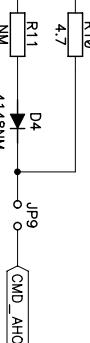
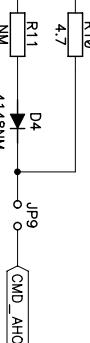
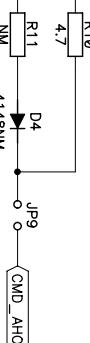
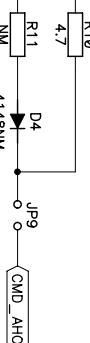
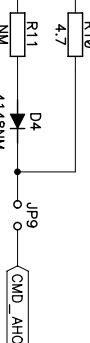
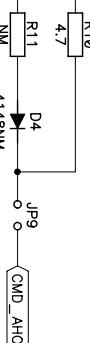
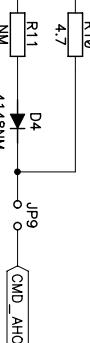
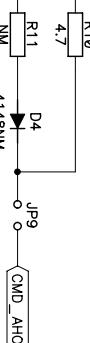
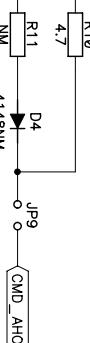
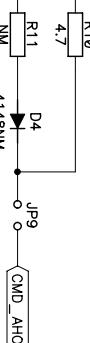
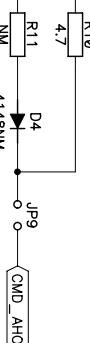
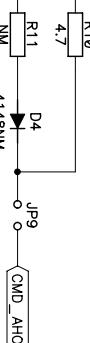
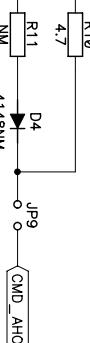
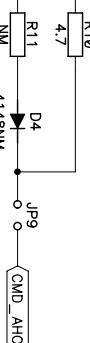
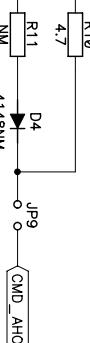
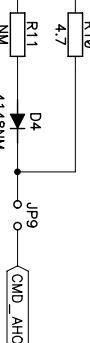
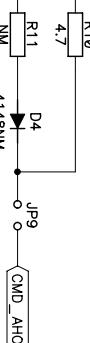
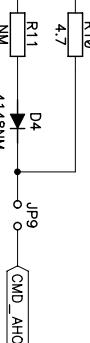
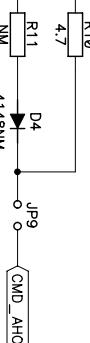
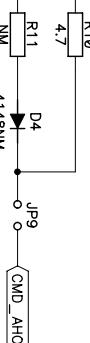
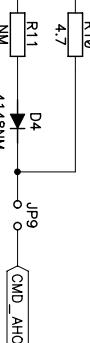
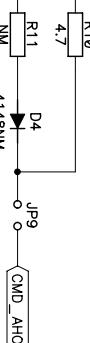
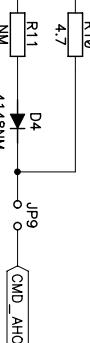
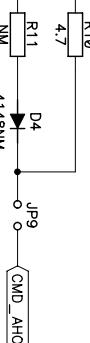
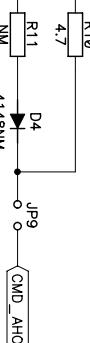
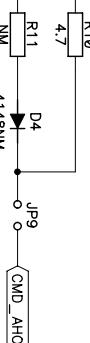
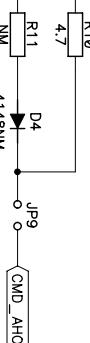
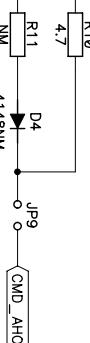
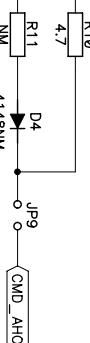
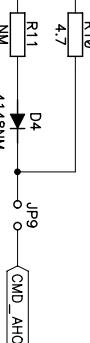
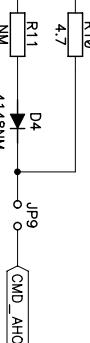
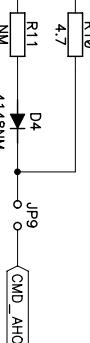
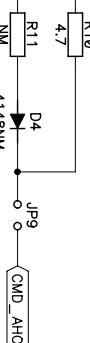
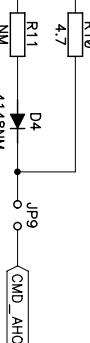
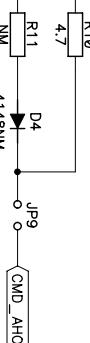
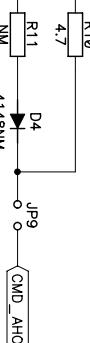
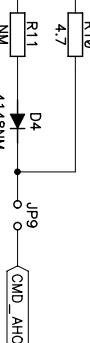
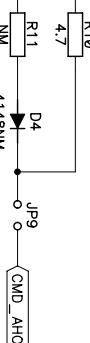
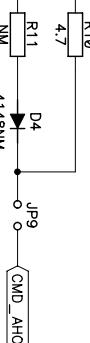
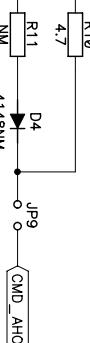
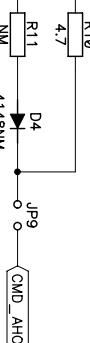
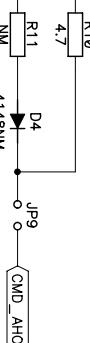
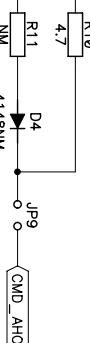
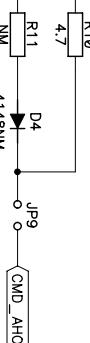
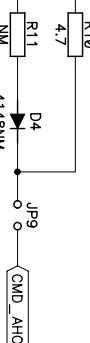
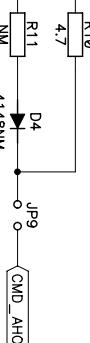
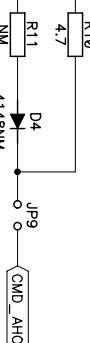
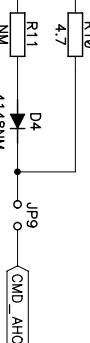
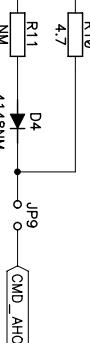
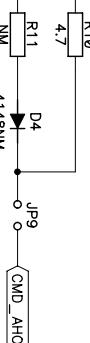
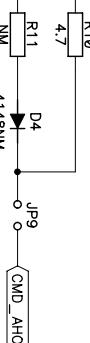
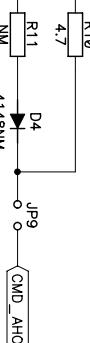
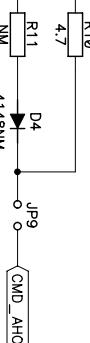
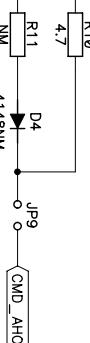
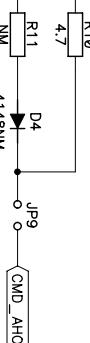
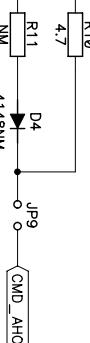
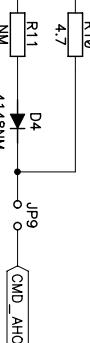
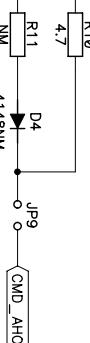
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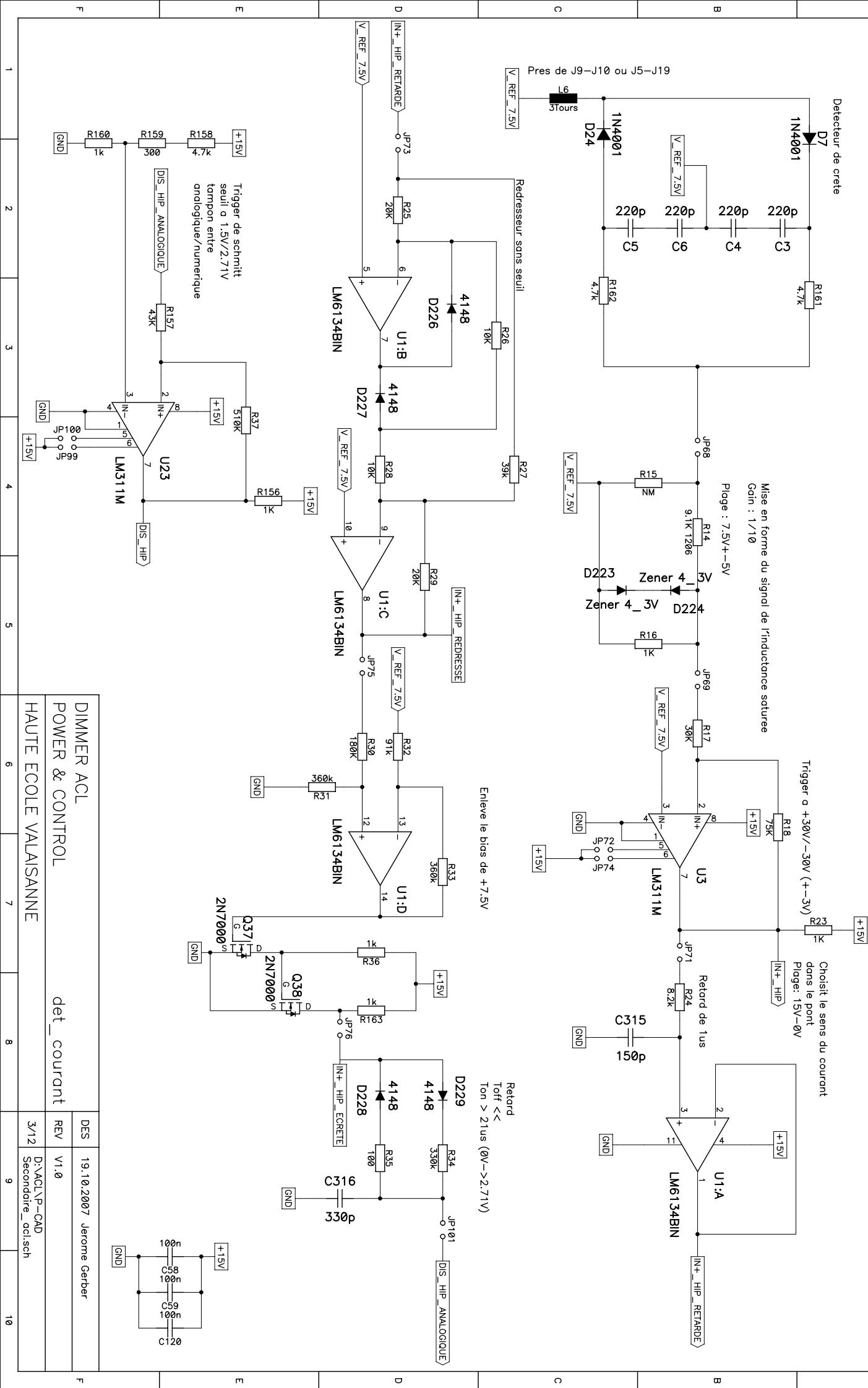


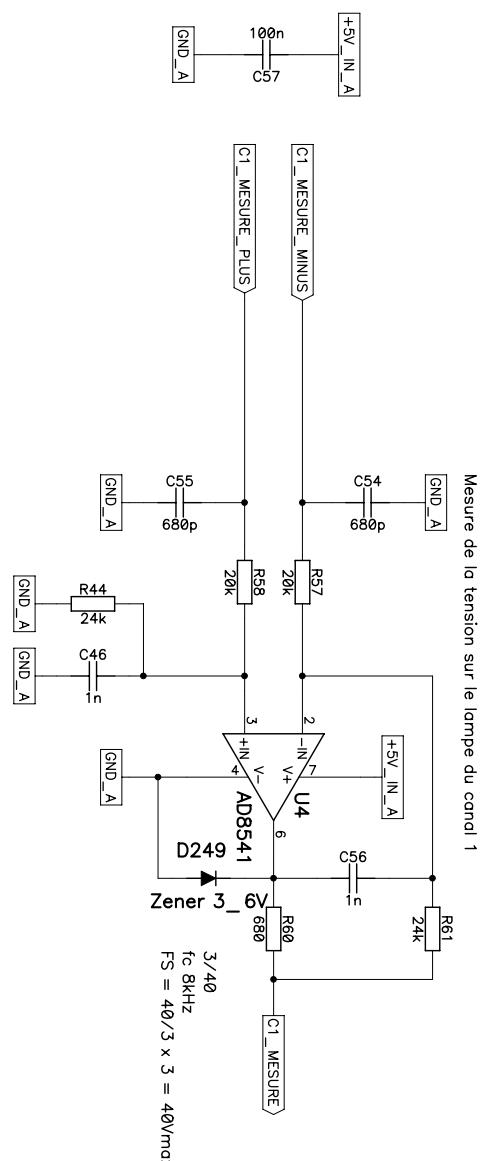
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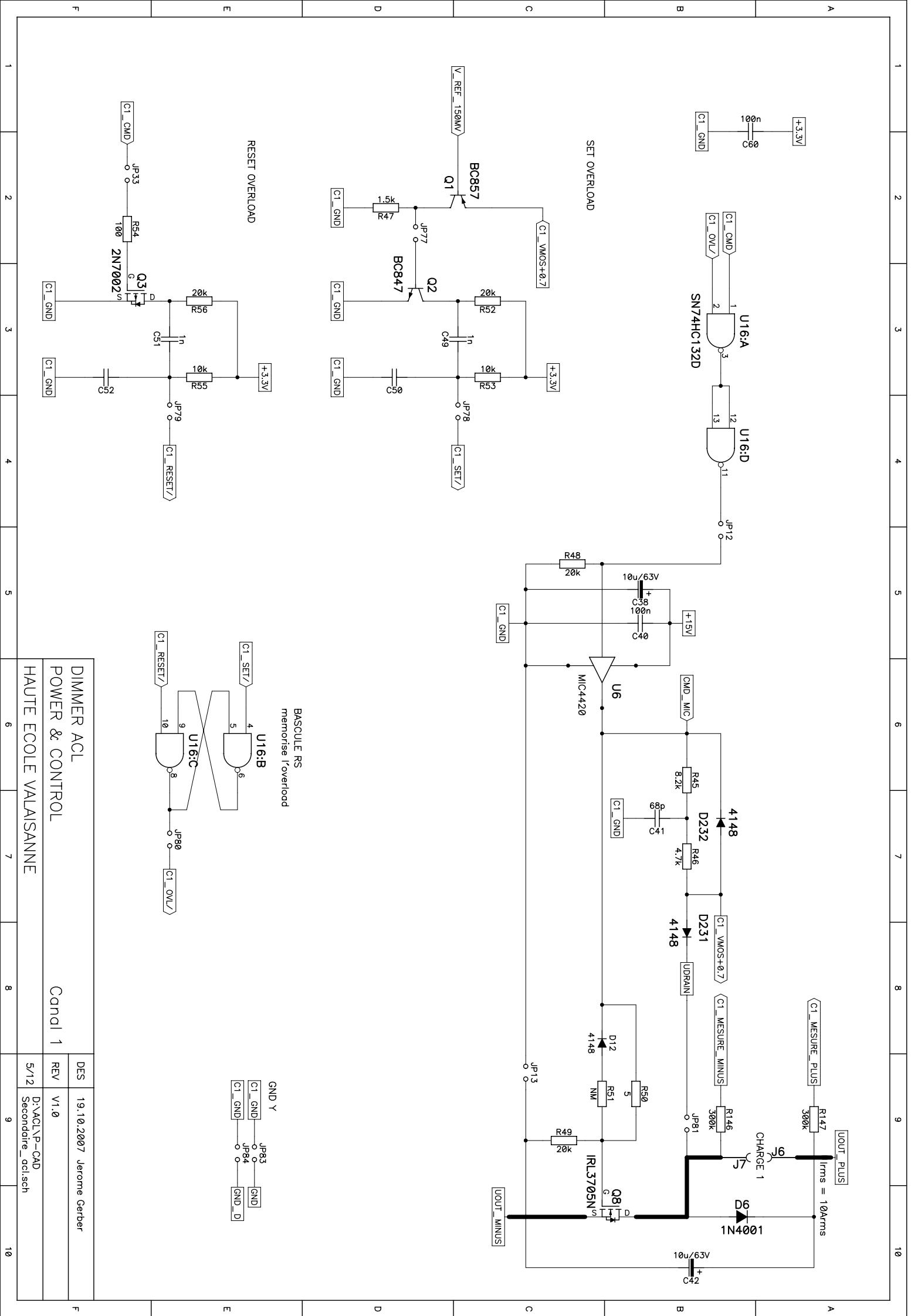
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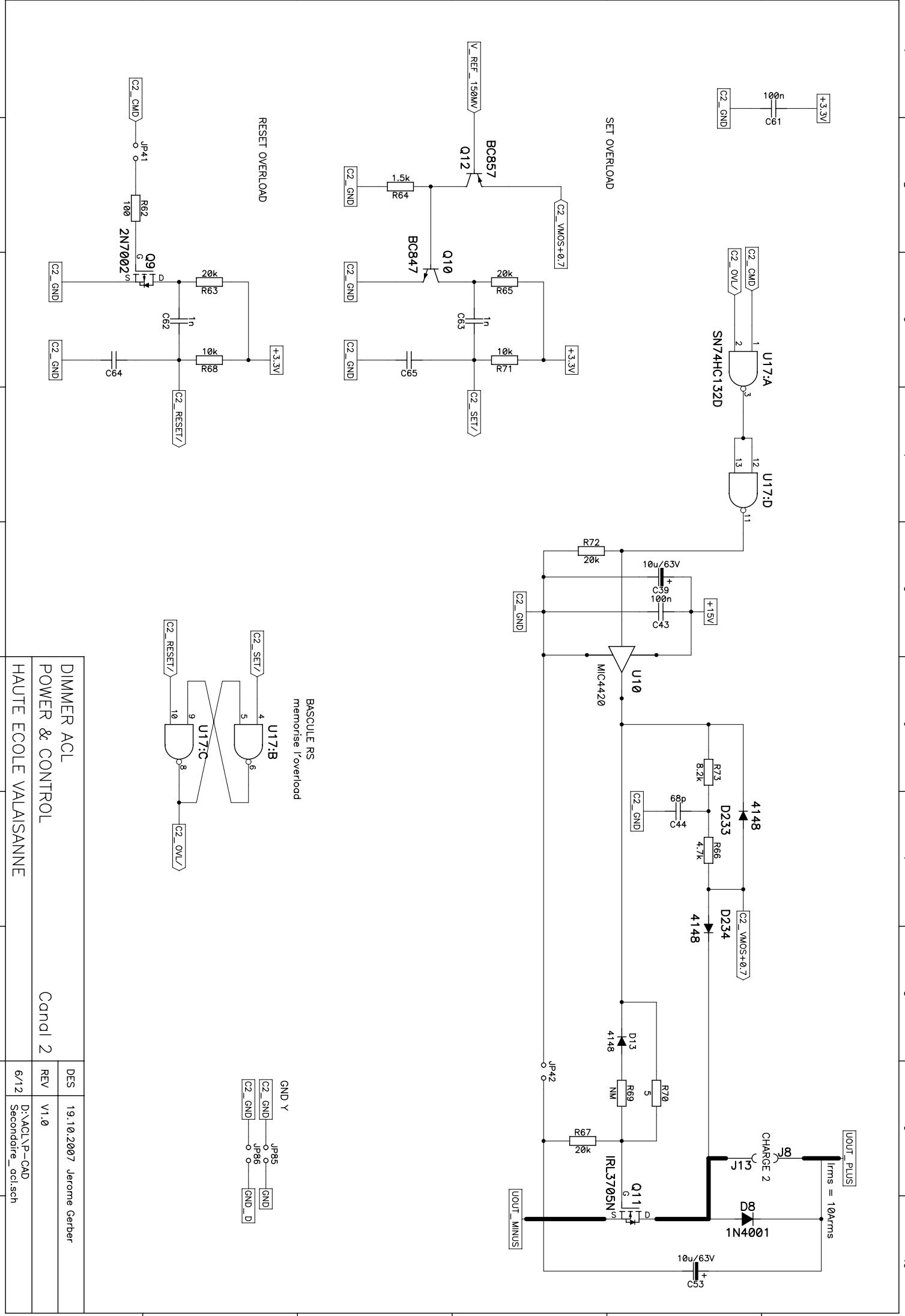


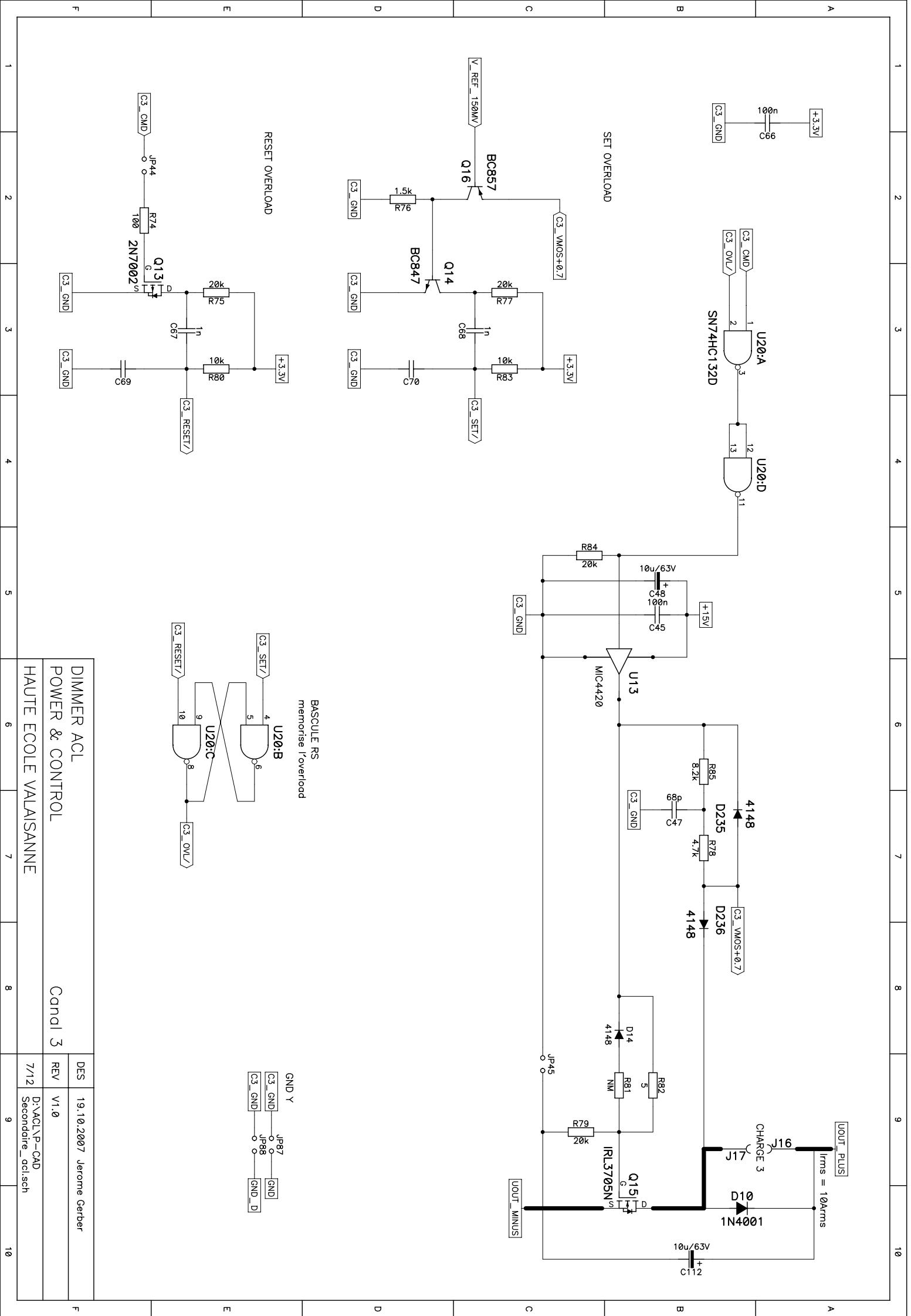


DIMMER ACL	DES	19.10.2007 Jerome Gerber
POWER & CONTROL	REV	V1.0
HAUTE ECOLE VALAISANNE	measures	4/12 D:\ACL\IP-CAD Secondaire_acl.sch

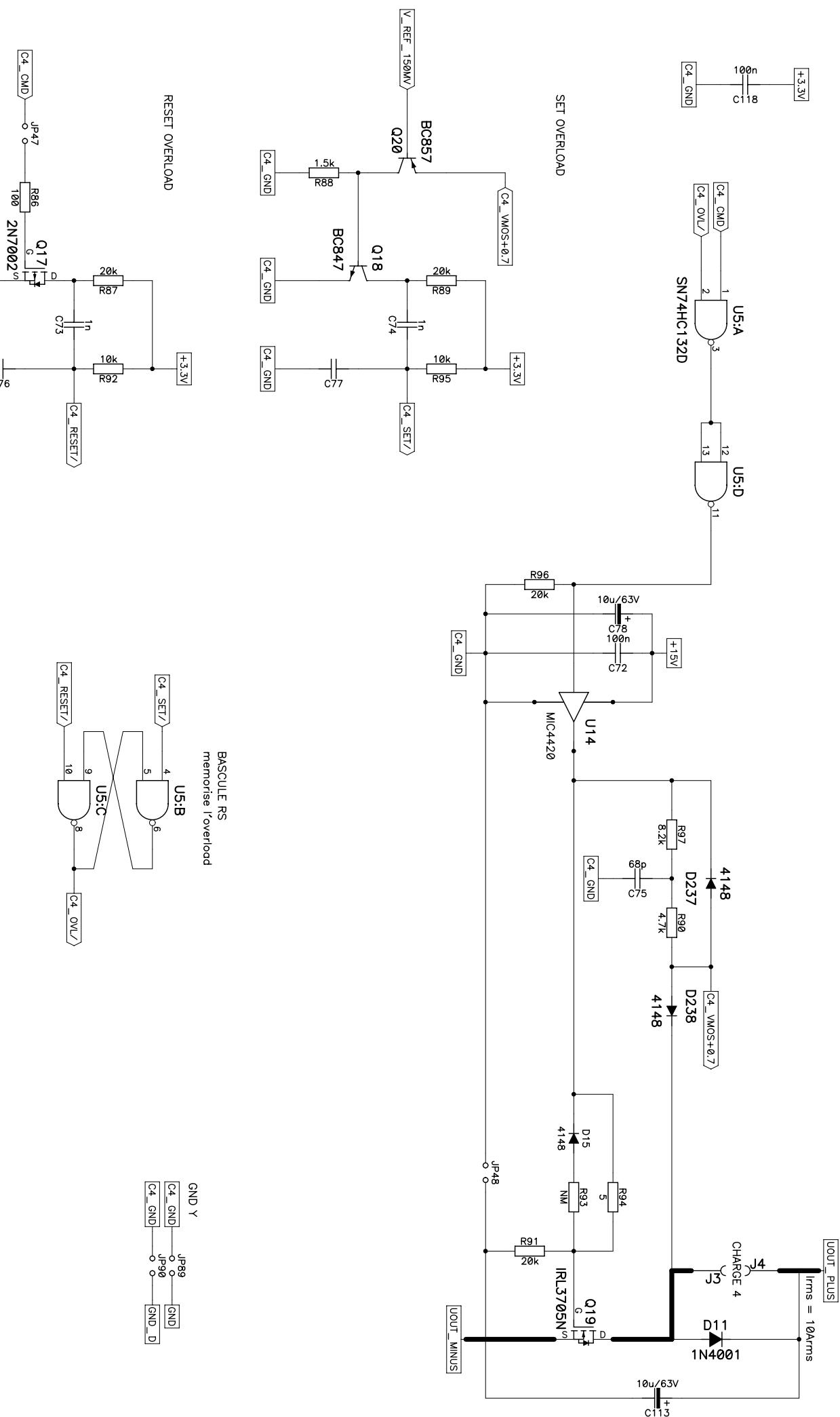


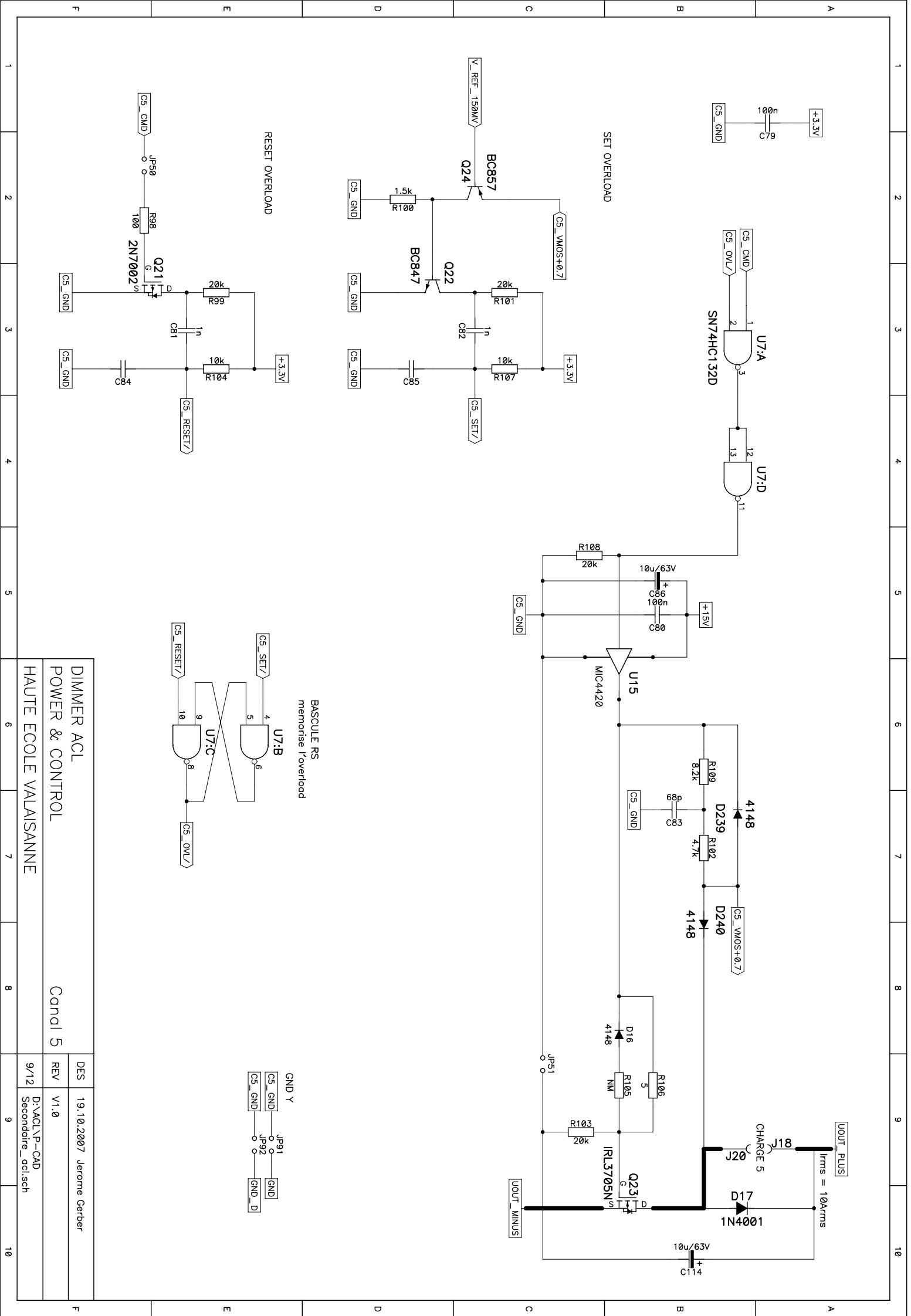
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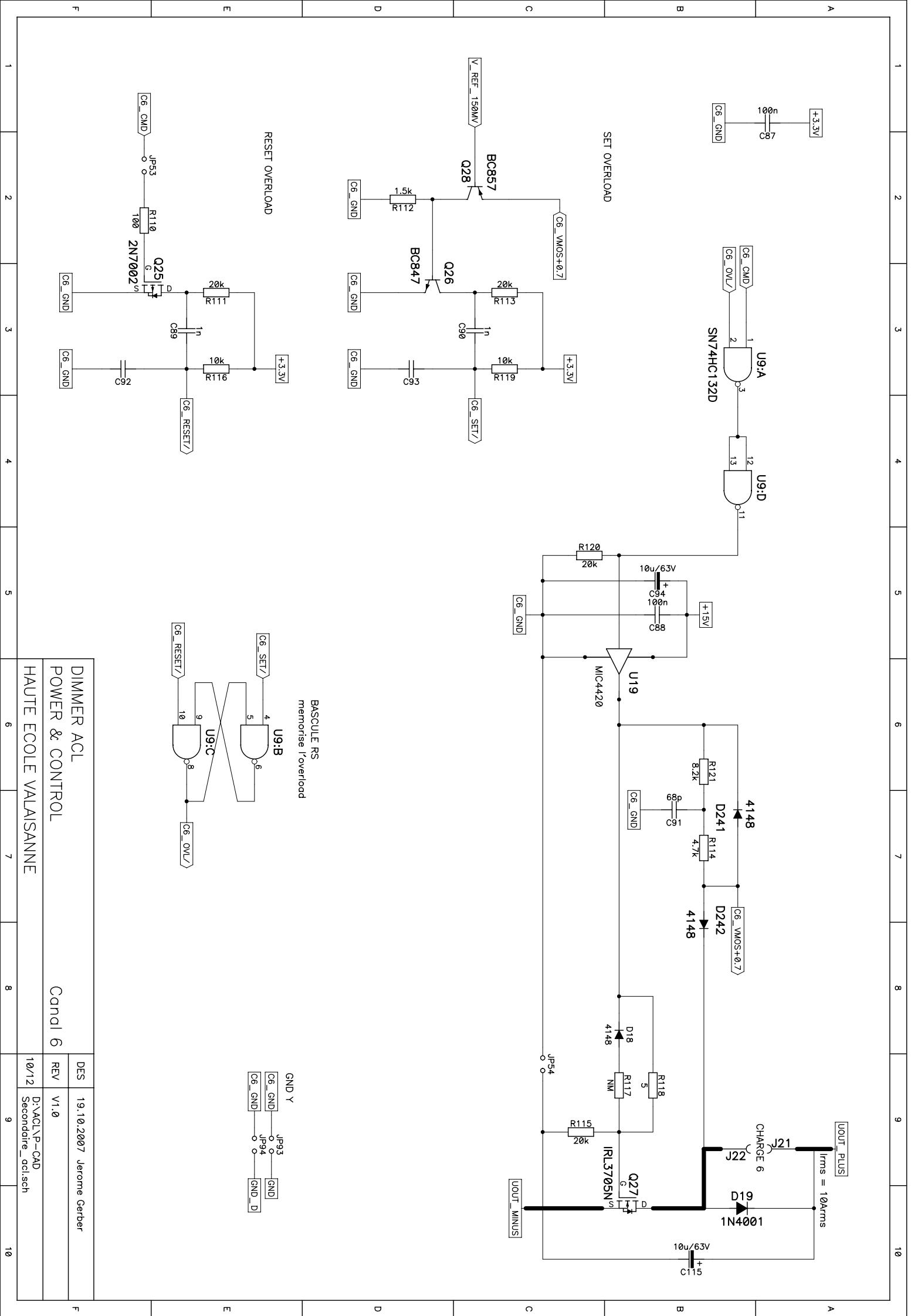




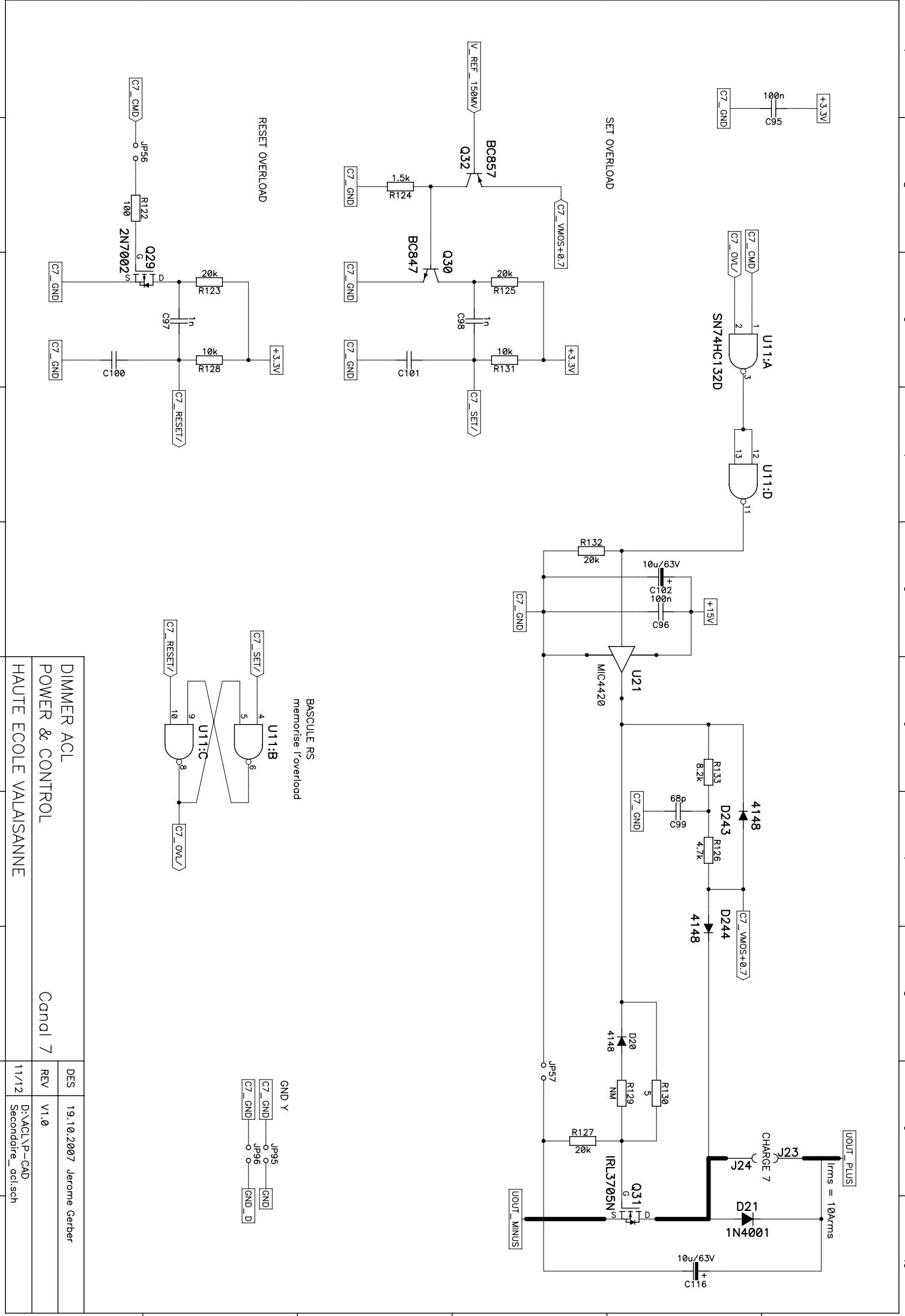
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1 2 3 4 5 6 7 8 9 10



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